

Stormwater nutrient attenuation by constructed wetland on the Swan Coastal Plain

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An Australian Government Initiative





Motivation

- Effect of urbanisation on water quality is a concern in Perth
 - Urban drainage contributes 180 tonnes of nitrogen and 16 tonnes of phosphorus to the Swan–Canning estuary annually (SRT, 2009)
- Substantial resources invested by water regulatory authorities to protect down stream water bodies by creating **constructed wetlands (CWs)**
 - Swan River Trust and partners have invested in several CWs as a part of **the Healthy Rivers Action Plan (HRAP)** to maintain water quality of the Swan–Canning estuary
 - Managed through the Drainage Nutrient Intervention Program (DNIP)



Background

Knowledge gaps:

- How does seasonality and antecedent dry condition affect the CW function?
- How does performance change over time?
- To what extent is nutrient reduction attributed to hydrological or biogeochemical processes?
 - *Considering inflow/ ungauged inputs/ GW connectivity/ rainfall event etc*
- What is particular role of compartments of CW to attenuate pollutant?
- Are there specific design elements that can improve performance on the Swan Coastal Plain (SCP)?



Aim

To assess effectiveness of **Wharf Street Constructed Wetland** through synthesis of long term monitoring data.

- Focusing on nutrient attenuation by different compartments

Study site:

- Situated in Cannington
- Started operation in 2009
- Multiple surface flow (SF) and subsurface flow (SSF) systems
- Subsurface compartments were constructed of recycled concrete material (RCM)
- Due to alkalinity problem, RCM were replaced with laterite in June 2012. SSF were then connected to rest of wetland





Nutrient attenuation calculation

Standardised delta concentration (SDC):

Because of ungauged input, we estimated the *standardised delta concentration (SDC)* - difference in nutrient concentration between inlet (C_{in}) & outlet (C_{out})

$$SDC (\%) = (C_{in} - C_{out}) / C_{in}$$

To account for effect of ungauged flows we also computed a modified version

$$SDC_{ave} (\%) = (*C_{in} - C_{out}) / *C_{in}$$

* C_{in} is average nutrient concentration of different inlets

Event mean concentration (EMC) and load attenuation:

During event sampling (simultaneous flow and nutrient concentration measurement)

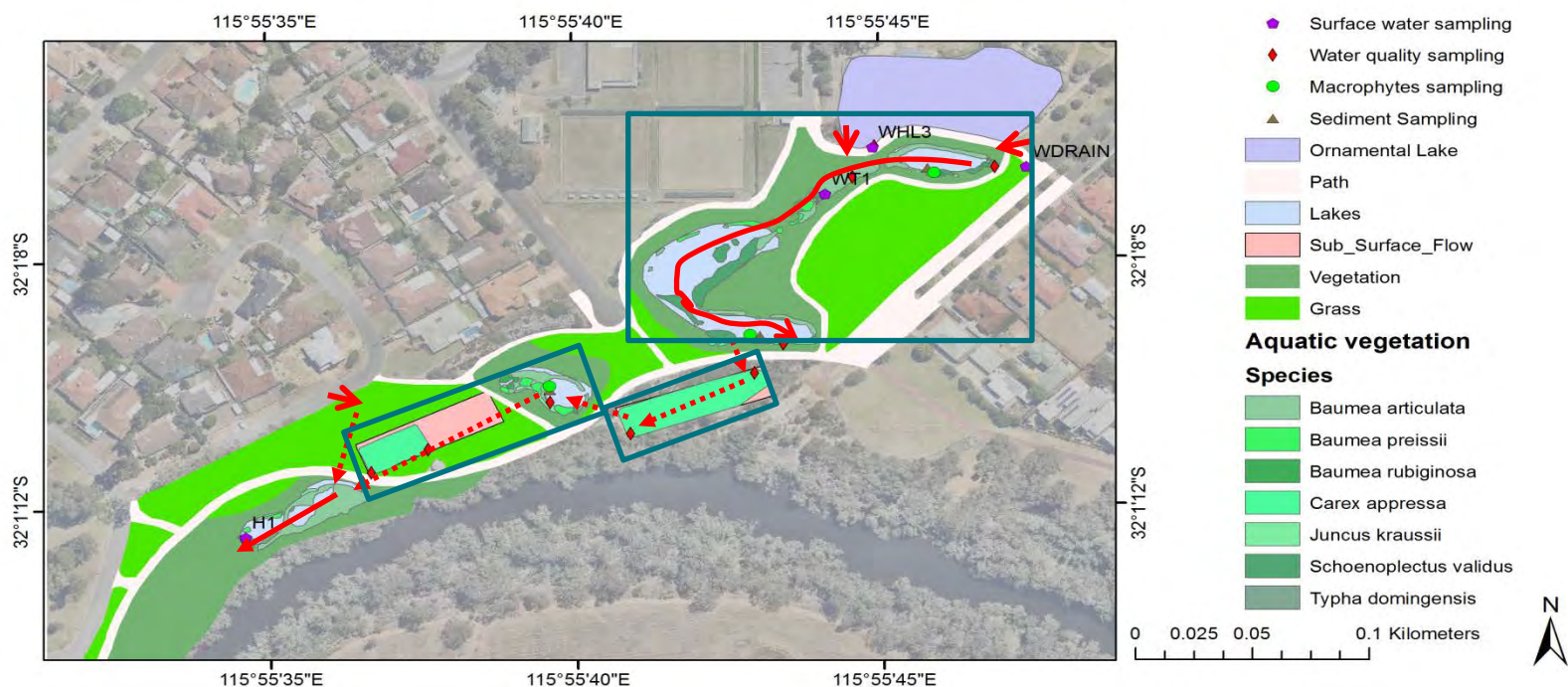
$$EMC (mg/L) = \sum_{i=1}^n V_i C_i / V$$

V_i is volume proportional to the flow rate at time i , C_i is nutrient concentration at time i , n is total number of samples, V is total runoff volume per event

$$\text{Load attenuation (\%)} = \frac{\sum \text{Inlet loading} - \sum \text{Outlet loading}}{\sum \text{Inlet loading}}$$



Wharf Street Constructed Wetland

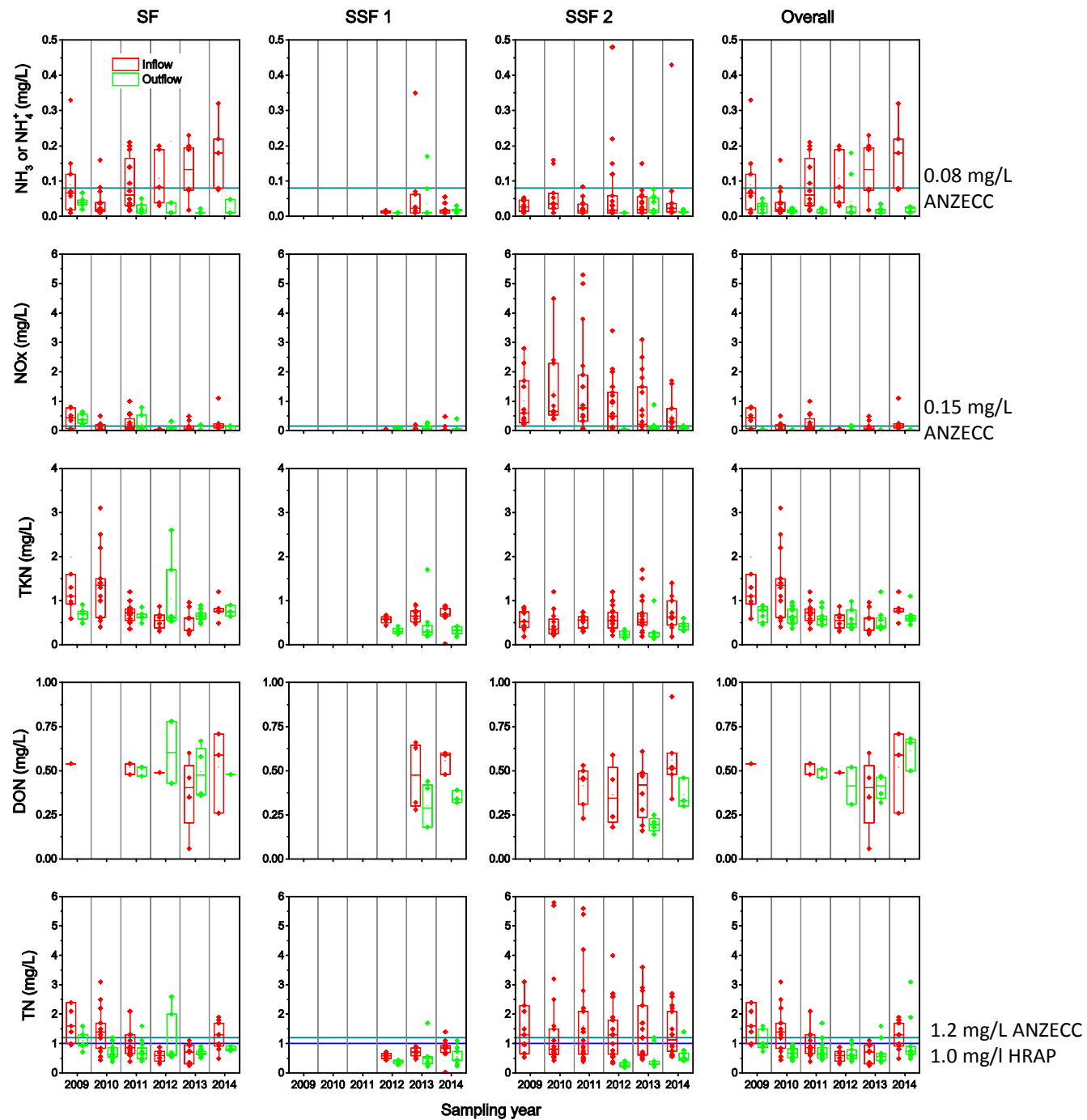


Compartments:

- 1: Surface flow (SF) 2: Laterite subsurface flow system 1 (SSF 1)
3: Laterite subsurface flow system 2 (SSF 2) 4: Overall system

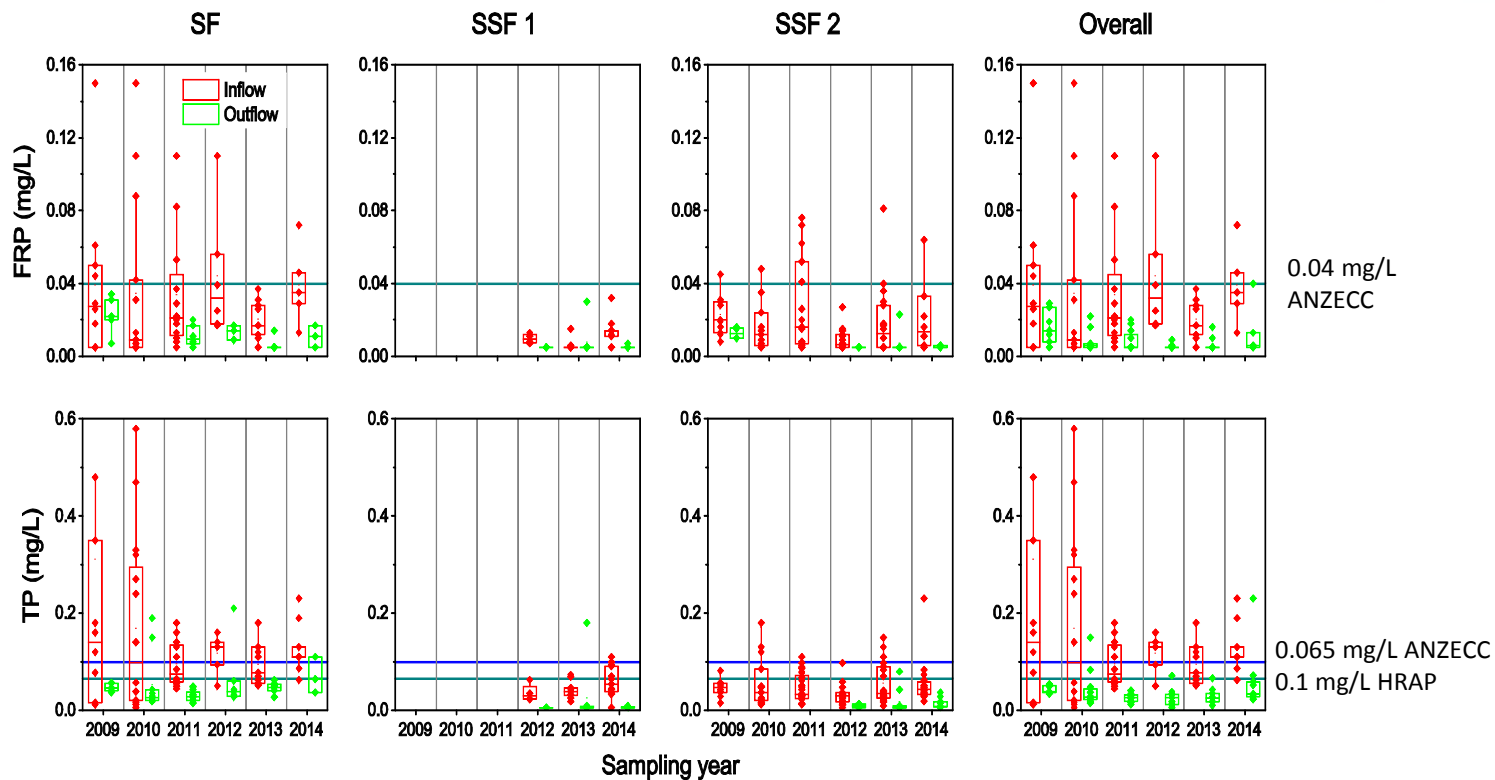
Nutrient dynamics

N species

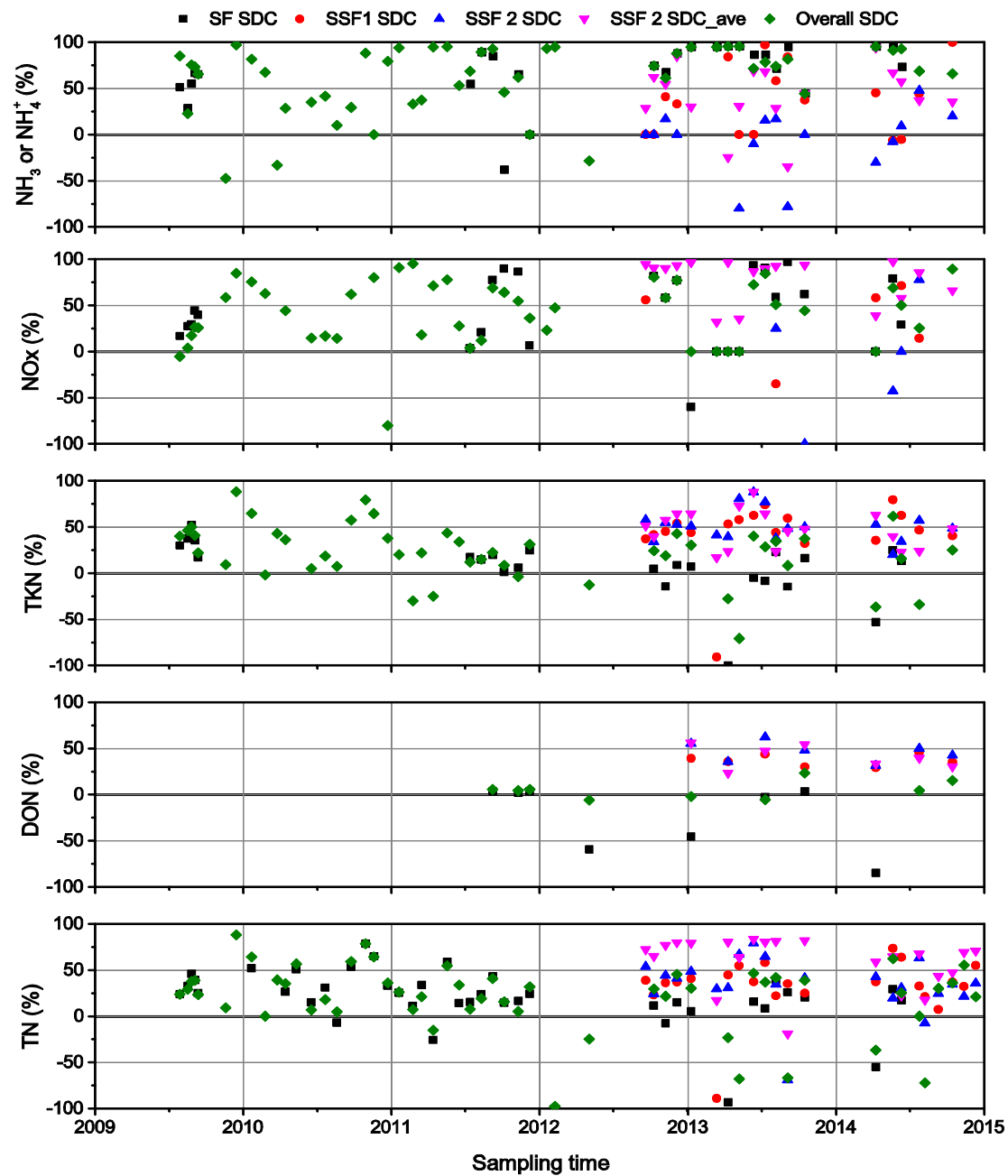




Nutrient dynamics - P species



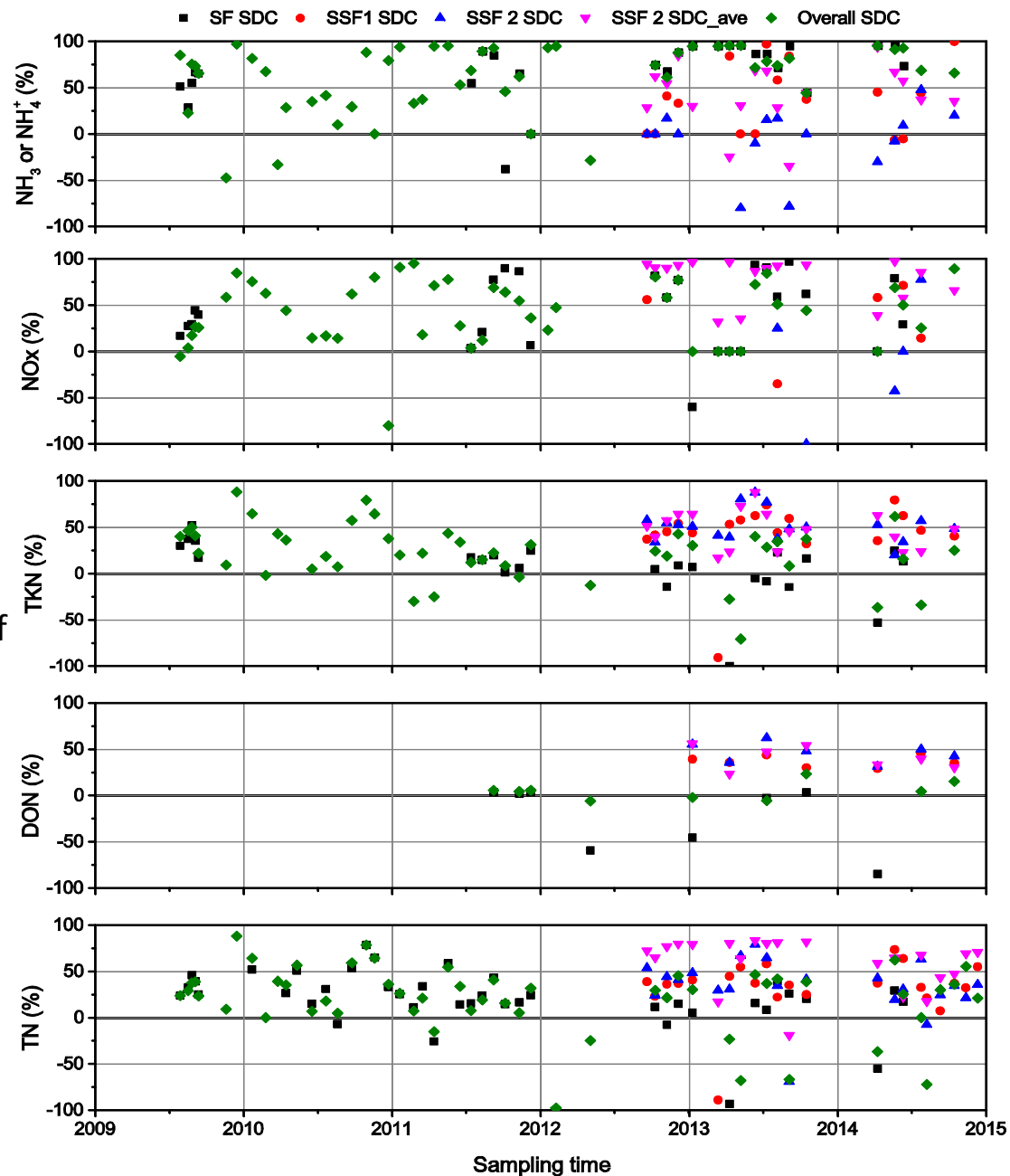
SDC (%) - N species



SDC (%) - N species

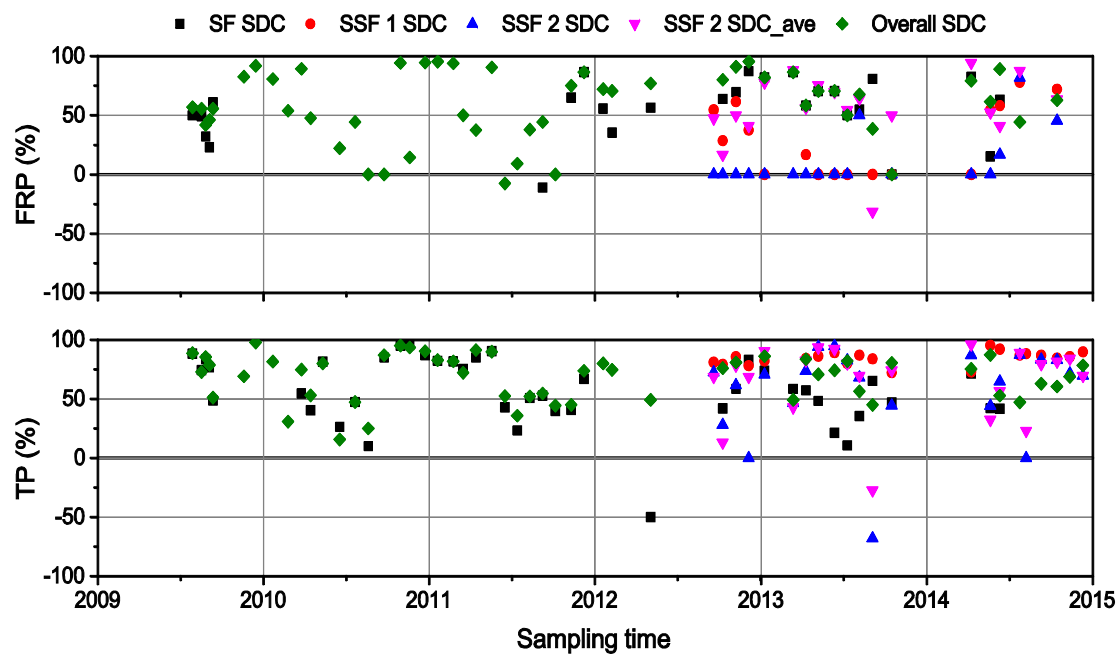
Findings - Nutrient attenuation

- Significant concentration attenuation for TN and DIN
- Up to 78% attenuation for TN by SF
- Up to 73% attenuation for TN by SSF
- Up to 88% attenuation for TN by WSCW
- Limited attenuation during high flows due to short retention time
- High attenuation during dry period
- Variable significance and contribution of ungauged sources depending on antecedent condition
- Disproportionate role of first SF in total attenuation
- SDC periodically negative for NOx in SSF 1 and SSF 2





SDC (%) - P species

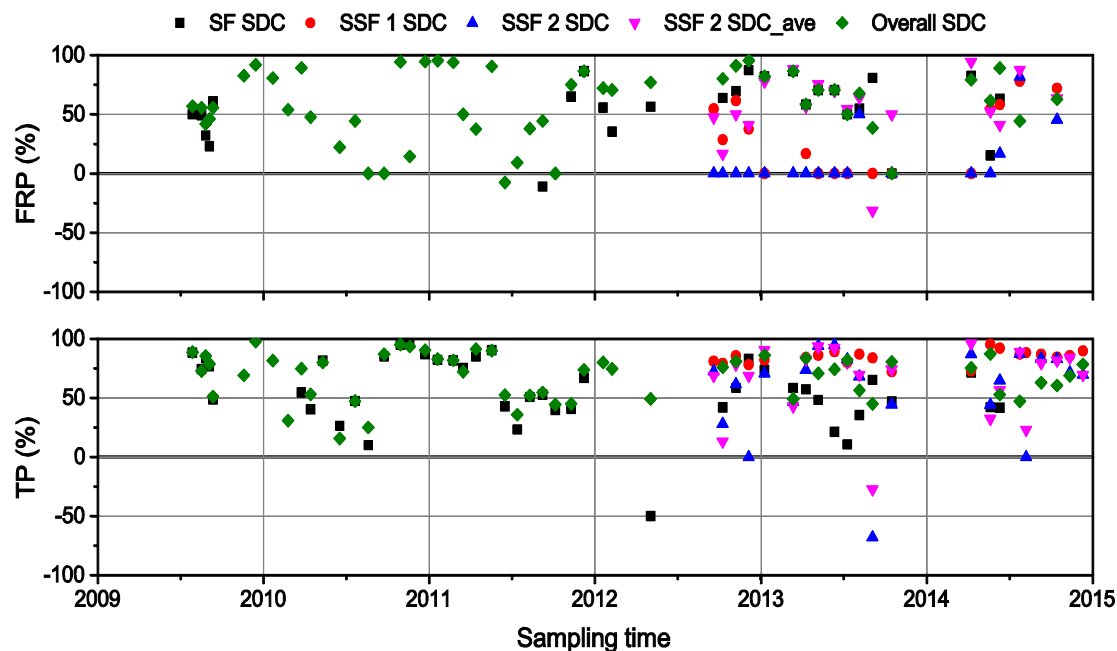




SDC (%) - P species

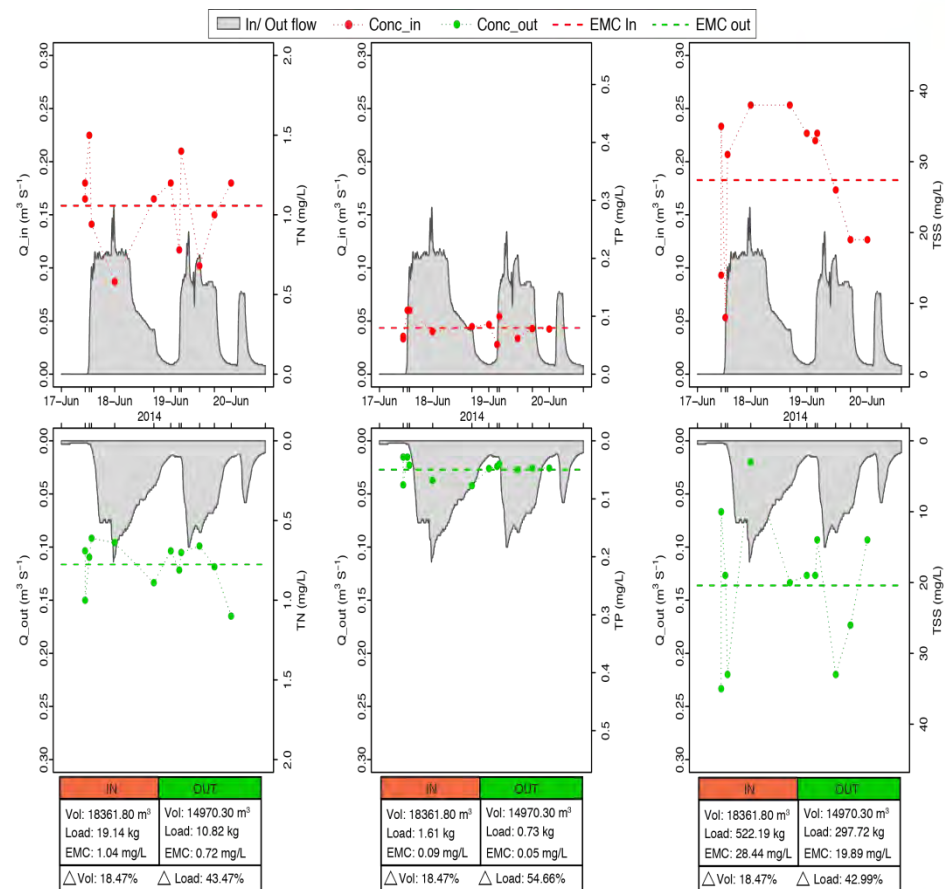
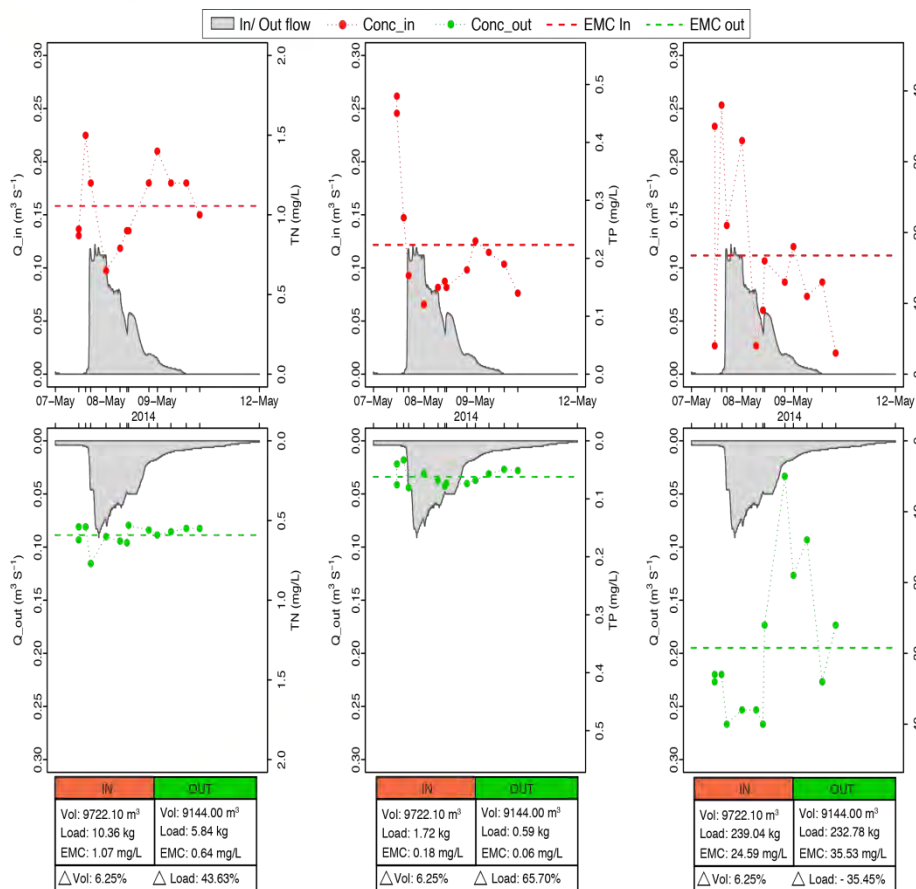
Findings - Nutrient attenuation

- Significant concentration attenuation for FRP and TP
 - Up 95% attenuation for TP by SF
 - Up 98% attenuation for TP by SSF
 - Up 95% attenuation for TP by WSCW
- High attenuation during dry period
- SSF compartments are more effective for P attenuation than SF





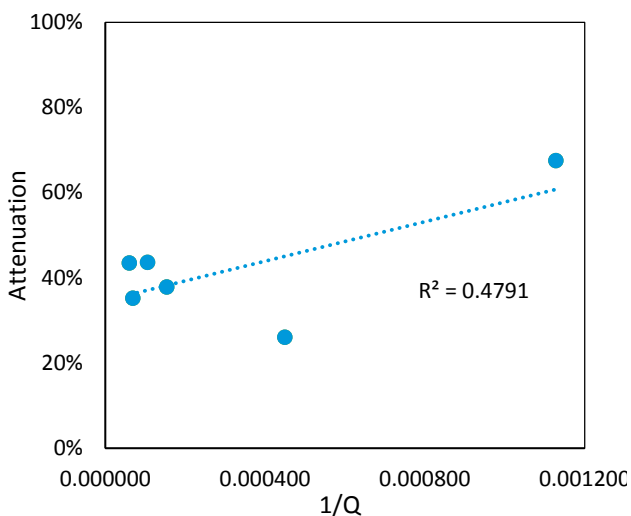
Event sampling-load calculation



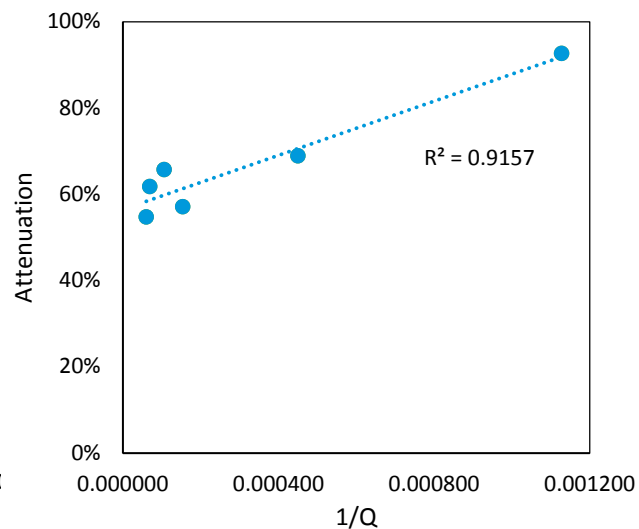


Nutrient attenuation as a function of travel time

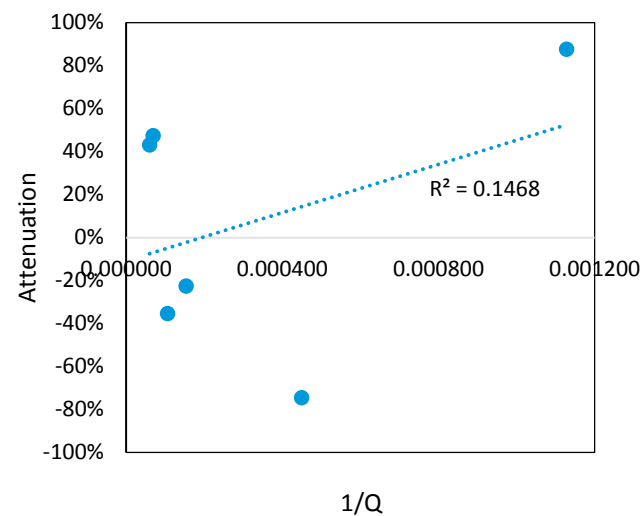
TN



TP



TSS





Conclusion

- Significant concentration attenuation for TN , TP, DIN and FRP - *base flow condition*
 - Up to 78% for TN, 95% for TP by SF
 - Up to 73% for TN, 98% for TP by SSF
 - Up to 88% for TN, 95% for TP by overall wetland
- Load attenuation ranged from 26-67% for TN and 54-92% for TP – *event flow condition*
- Attenuation increased during dry period
- SSF compartments are more effective for P attenuation than SF
- Variable significance and contribution of ungauged sources depending on antecedent condition
- Relatively consistent outlet concentration over last five years



Acknowledgement

- UWA SIRF
- CRC WSC
- Swan River Trust
- Department of Water, WA
- City of Canning
- Water Corporation, WA
- SERCUL
- Public Transport Authority
- Carlos Ocampo
- Ana Ruibal
- Hasnein Bin Tareque



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Thanks...





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An Ecohydrological Model Framework to Assist Constructed Wetland Design

WaterWays Seminar 1st May 2015



Jana Coletti
Matt Hipsey

Background: Anvil Way

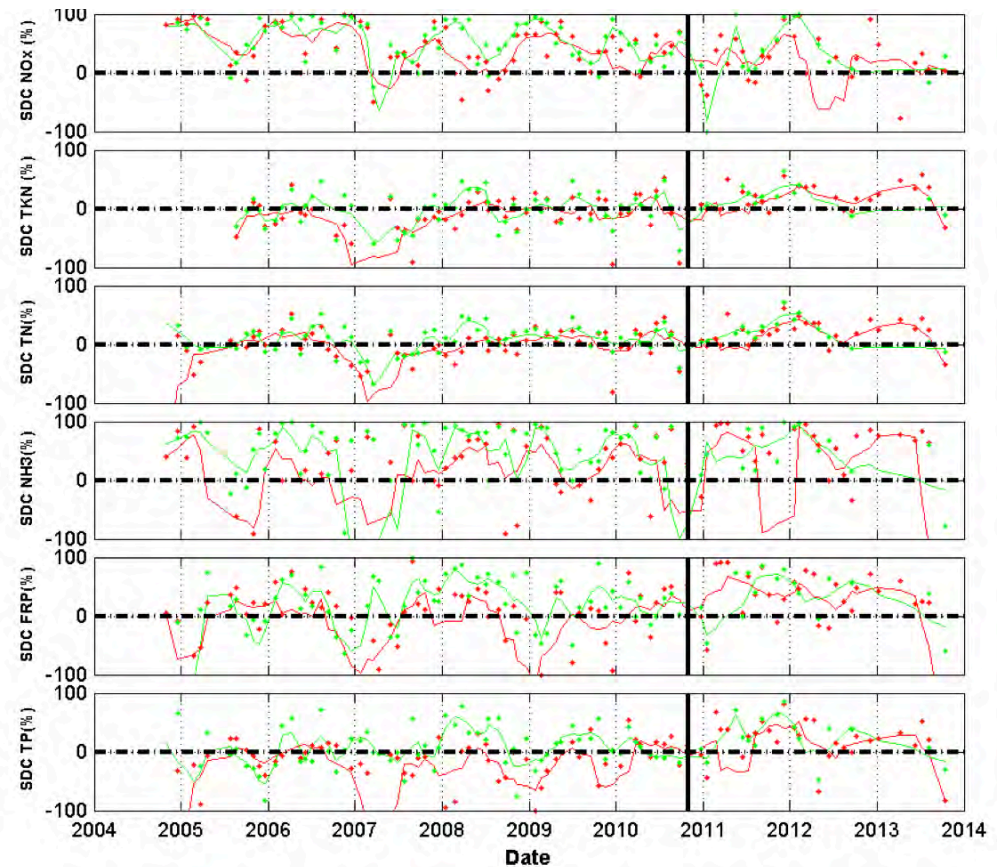


Performance of Anvil Way Compensation Basin restoration project

2004-2013



Variable nutrient reduction (+ve = loss)



Motivation

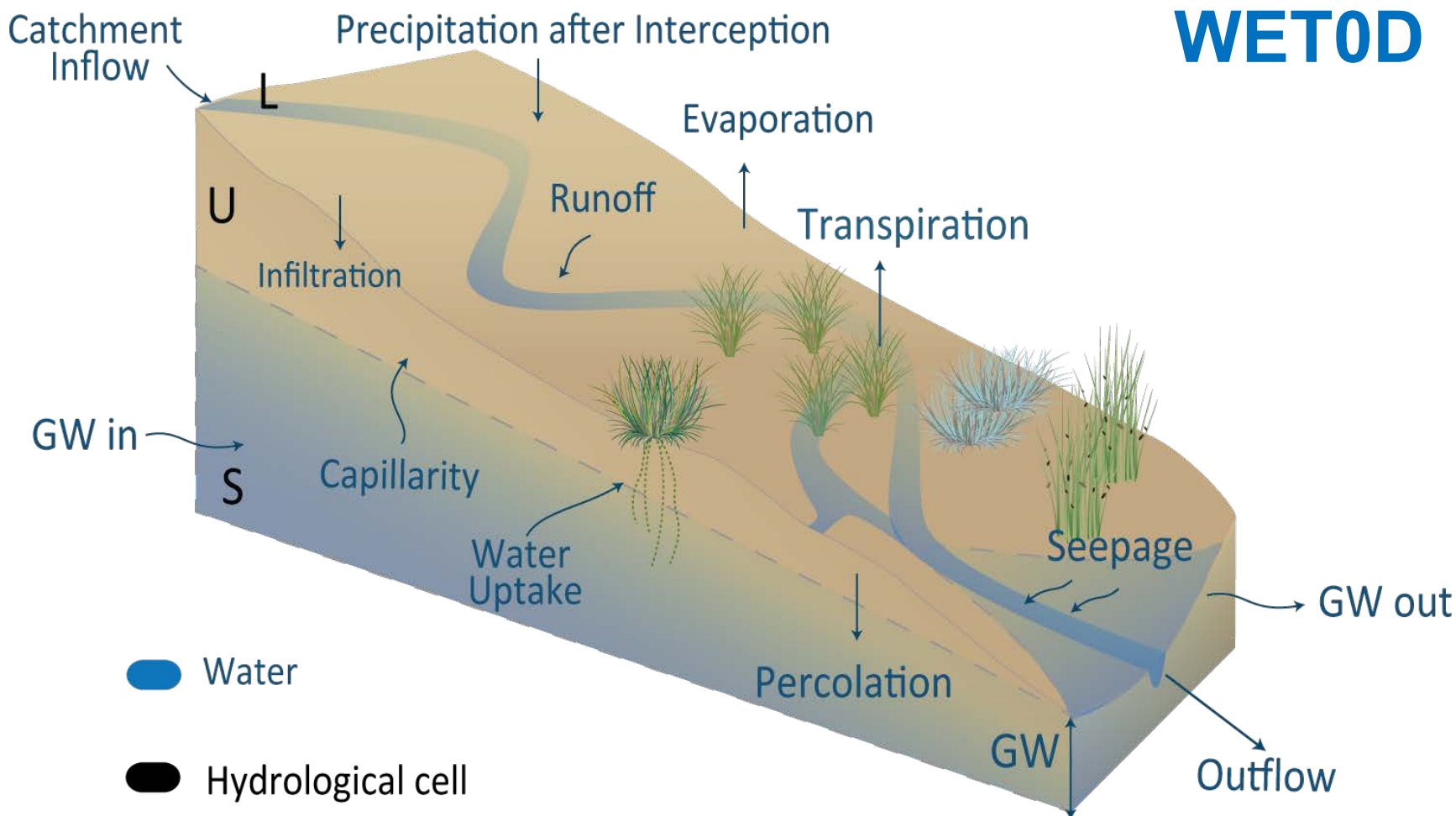
Ongoing questions

- Hydrological conditions X attenuating nutrients?
- Can we manage the wetland to improve its performance?
- What is the link between hydrological pathways and pollutant reduction?
- What is the significance of groundwater – how much comes in or out?
- How can we account for role of ungauged inputs?



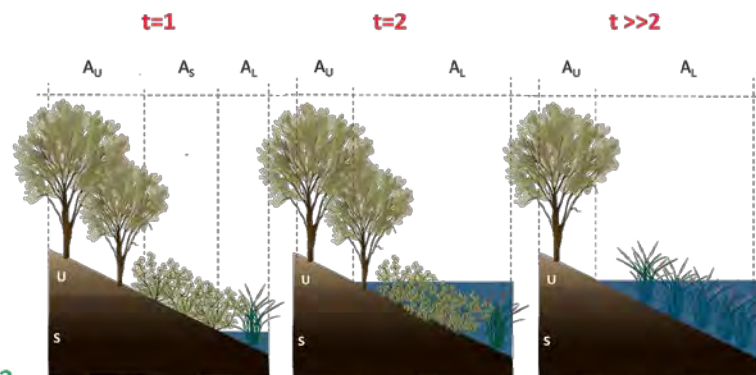
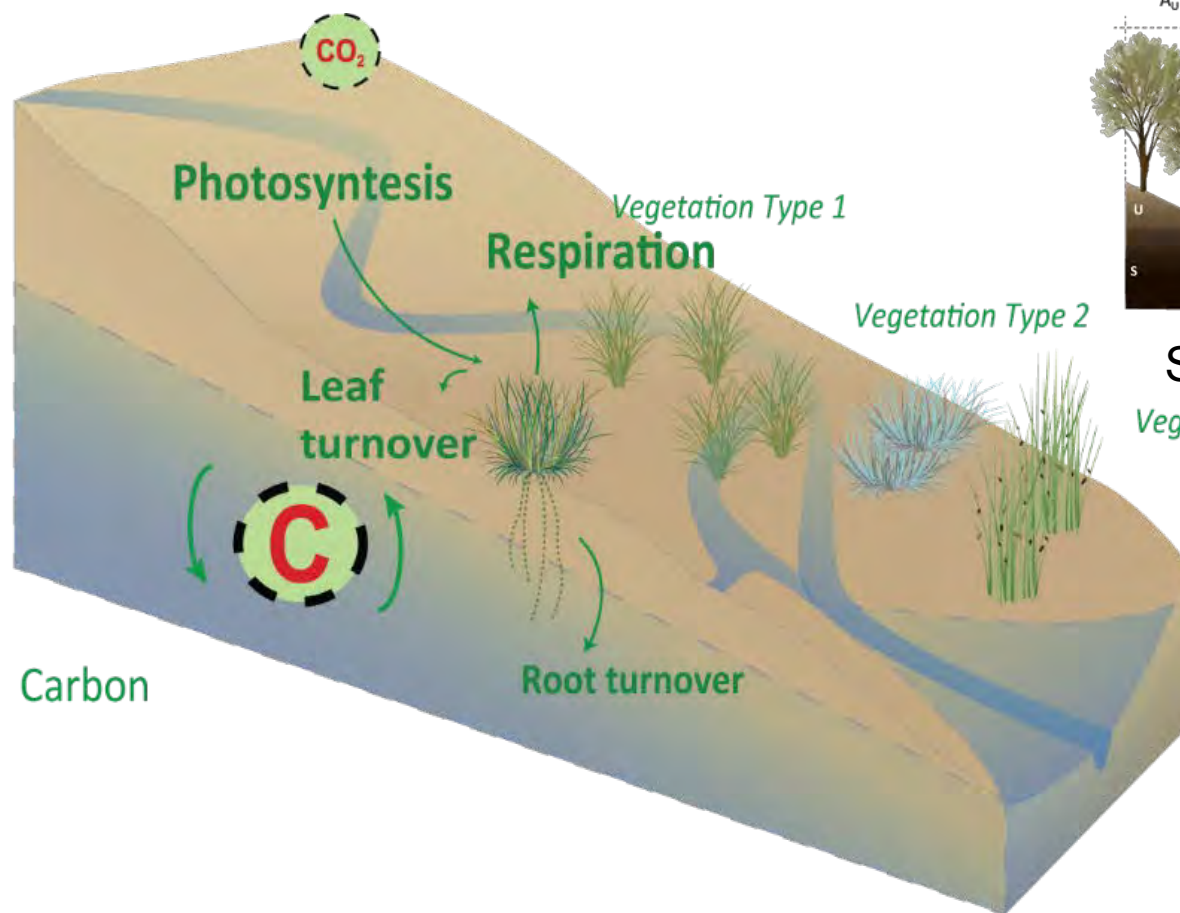
1. Ecohydrological Model

WETOD





1. Ecohydrological Model

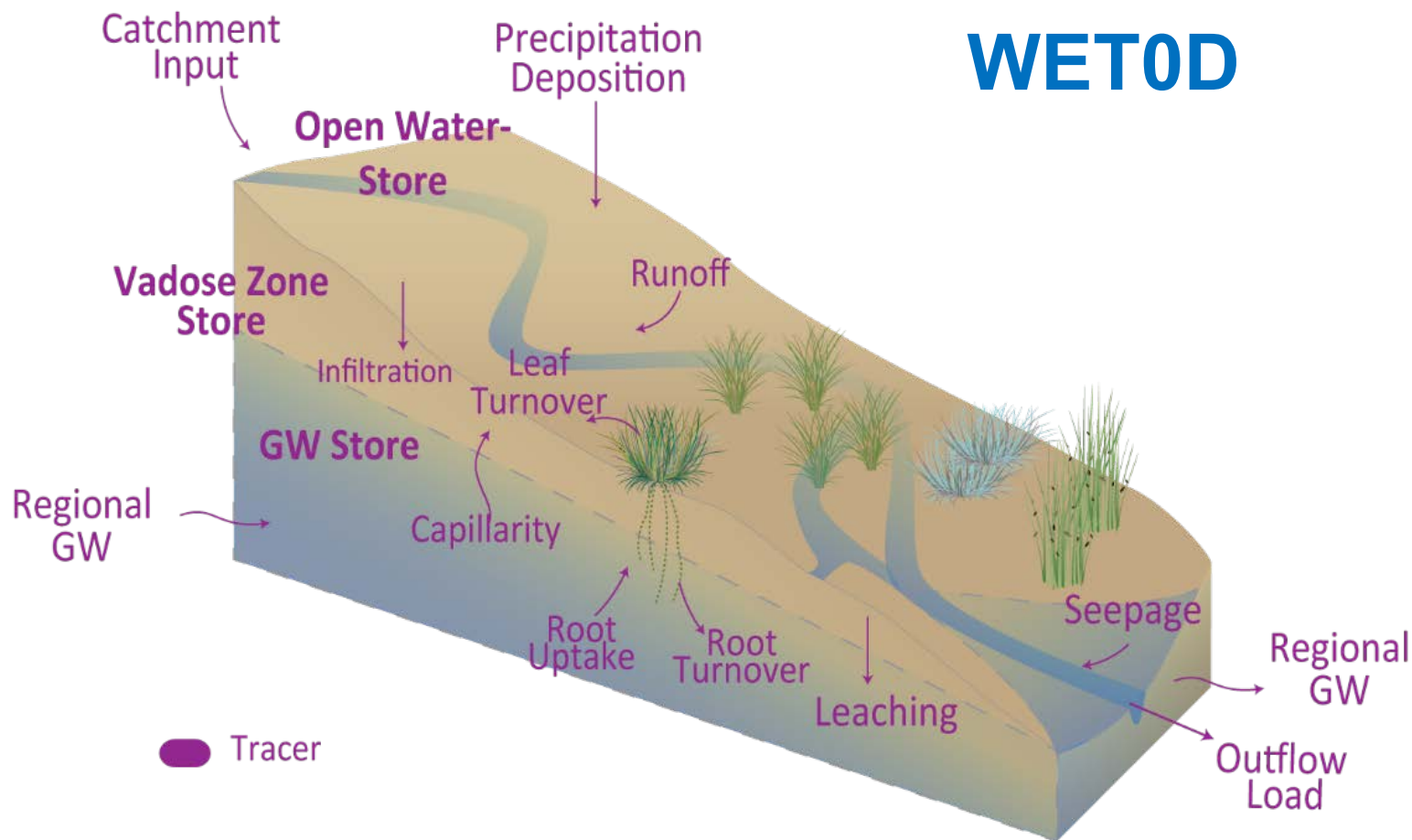


Simulating Vegetation Zonation
Vegetation Type 3

WET0D



1. Ecohydrological Model





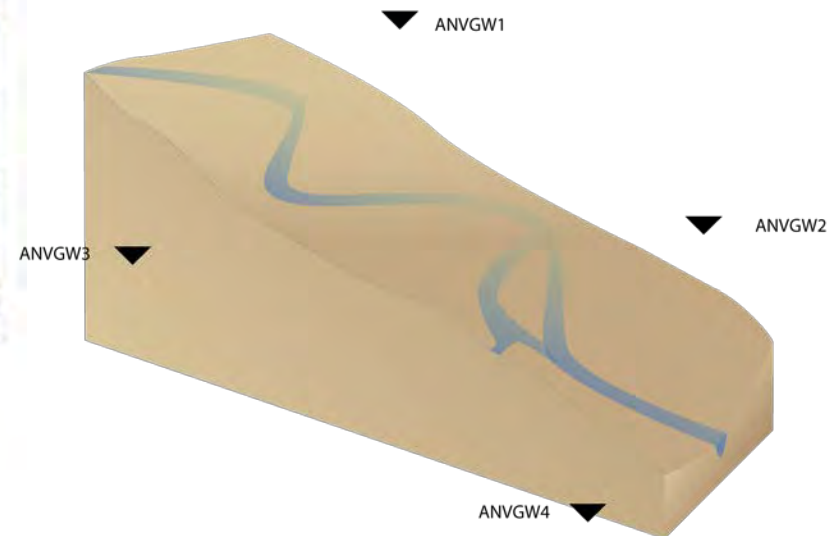
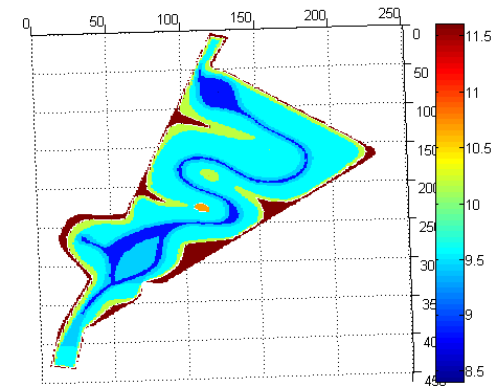
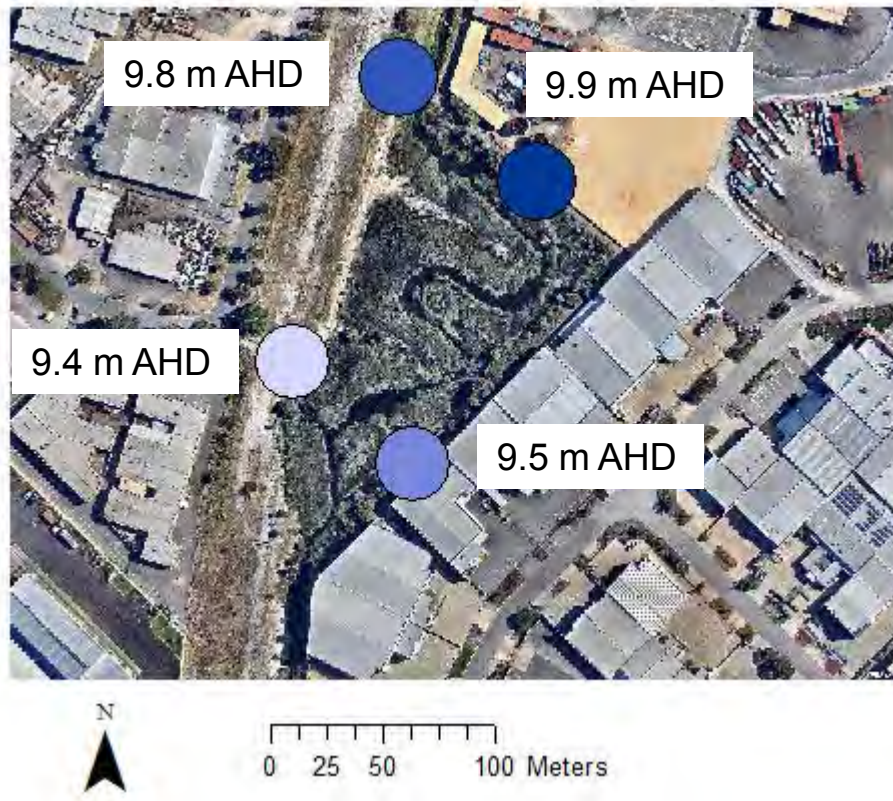
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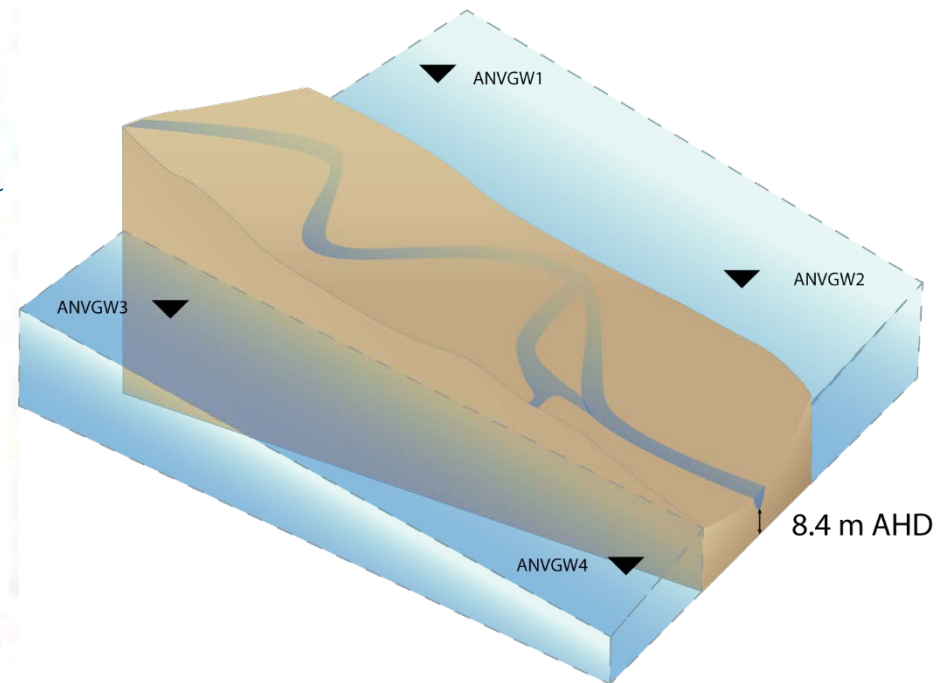
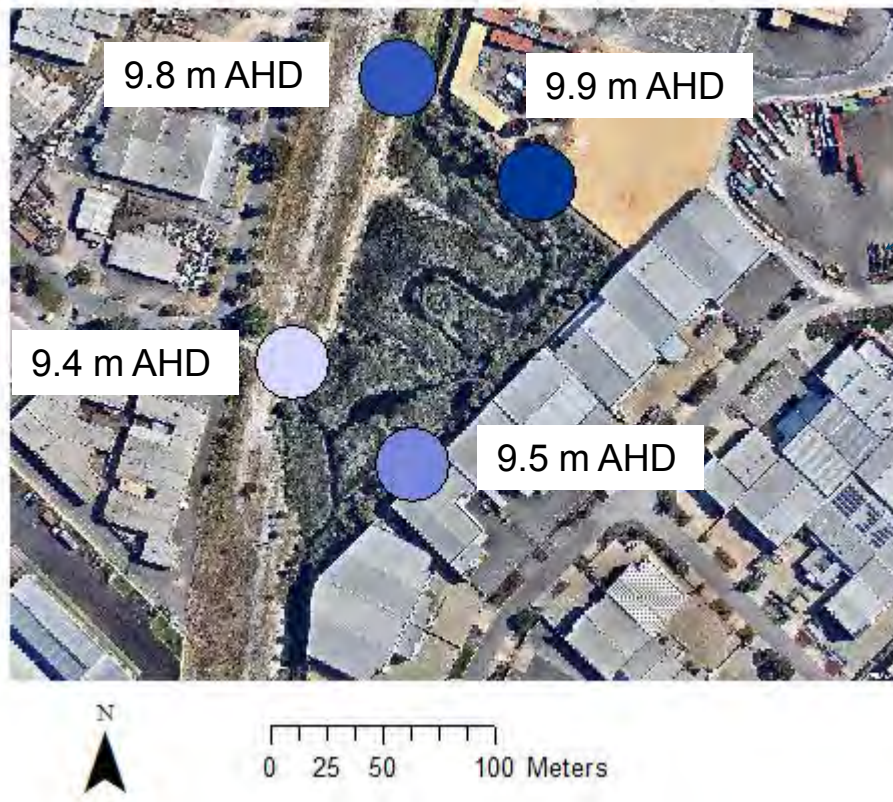


2. Application to Anvil Way CW





2. Application to Anvil Way CW





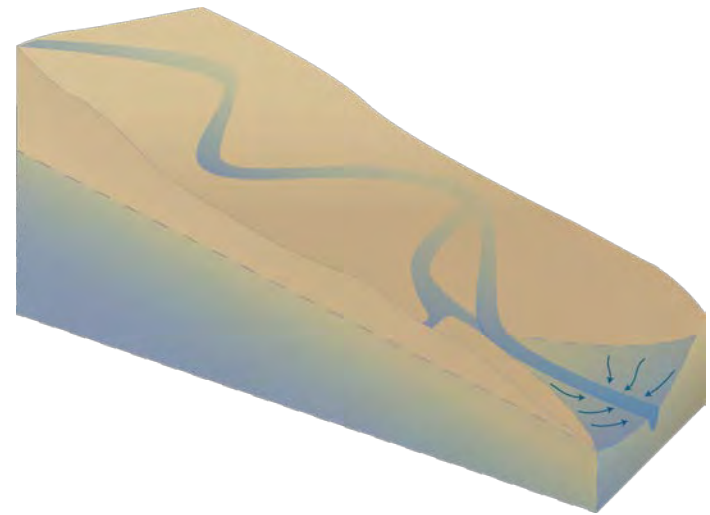
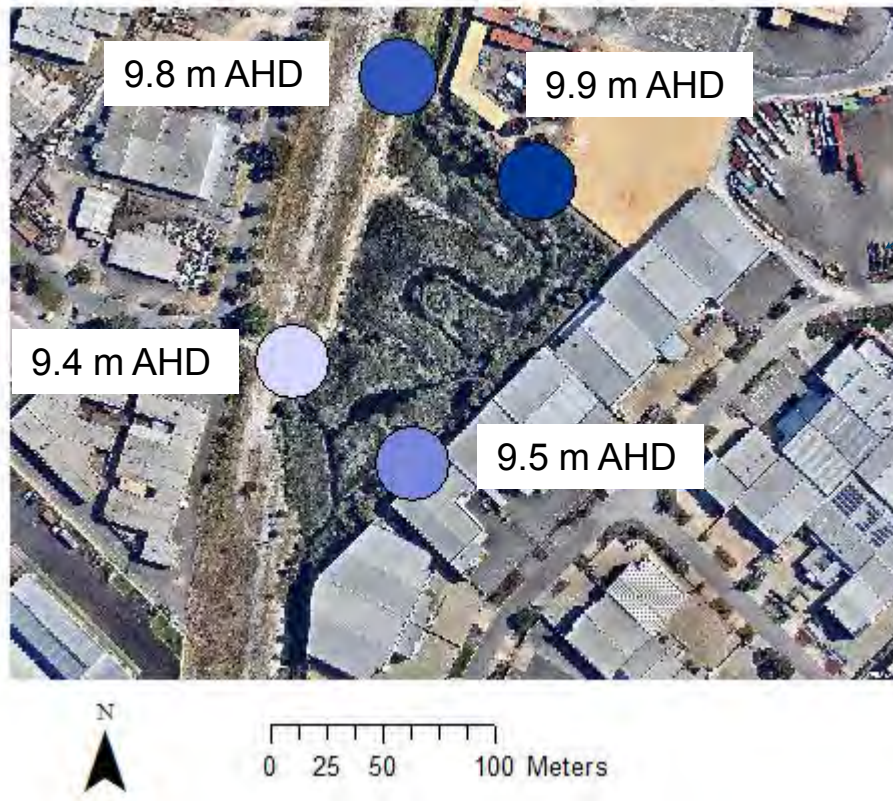
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2. Application to Anvil Way CW



Likely GW
contribution



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2. Application to Anvil Way CW



Anvil Main Inlet
Site 6162964
(Abernethy Road)

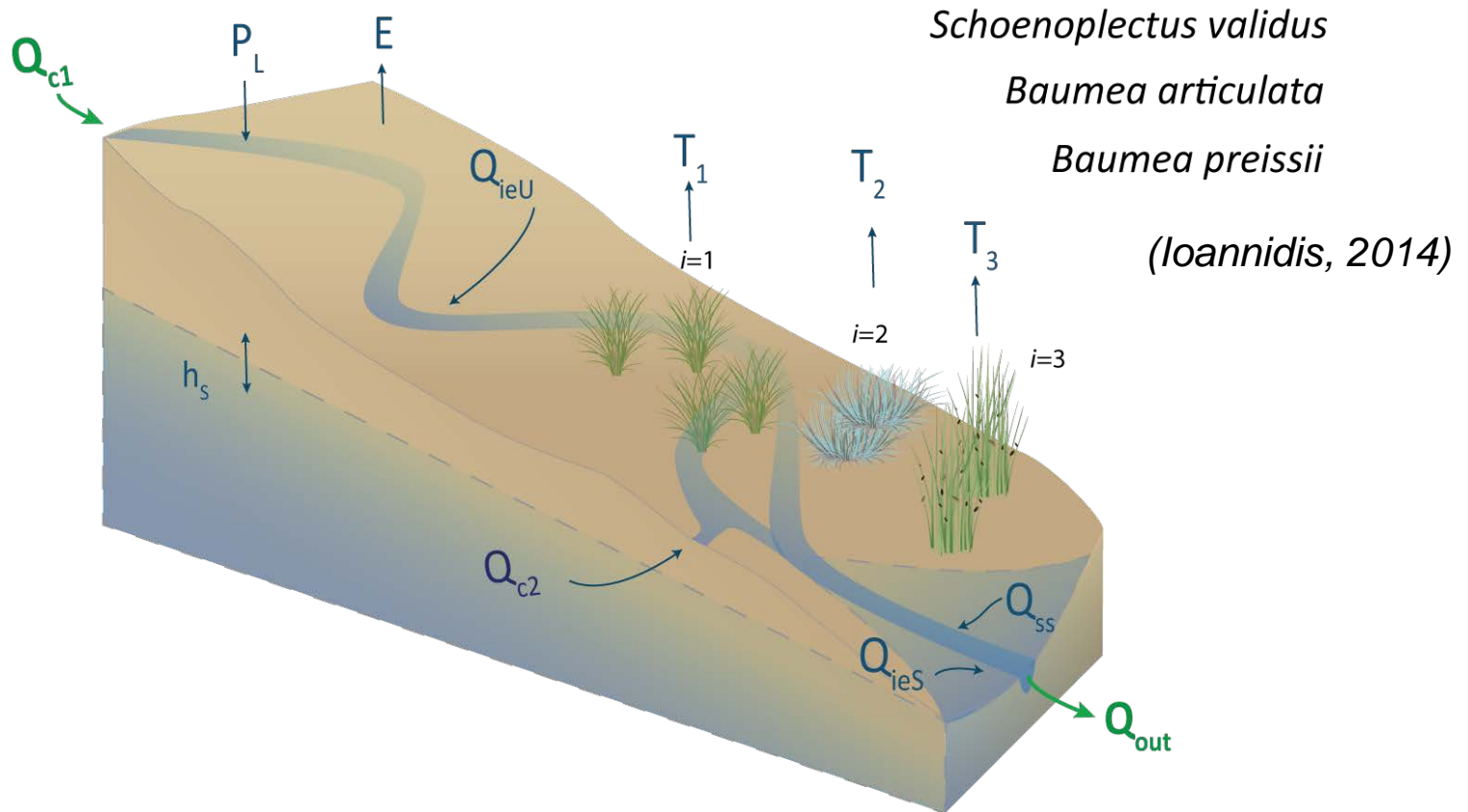
Mars St
Anvil Mid Inlet

Anvil Main
Outlet
Site 6162796

Ungauged
hydrological input



2. Application to Anvil Way CW



$$Q_{c1} + Q_{c2} + Q_{ieU} + Q_{ies} + Q_{se} + Q_{SS} + P_L = Q_{out} + \sum_{i=1}^3 \sum_{n=1}^3 T_{i,n} + \sum_{n=1}^3 E_n + \Delta S$$



2. Application to Anvil Way CW

$$Q_{ieU} = (P_U A_U - I)$$

$$Q_{ieS} = P_S A_S$$

$$E_L = k_E E_0 \left(1 - k_{LAI} \frac{LAI_L}{LAI_{max}}\right) A_L$$

$$E_U = \left(\frac{\theta}{\theta_{fc}}\right) E_0 \left(1 - k_{LAI} \frac{LAI_U}{LAI_{max}}\right) A_U$$

$$E_S = k_S E_0 \left(1 - k_{LAI} \frac{LAI_S}{LAI_{max}}\right) A_S$$

$$T_{i,n} = \sum_{i=1}^3 \Psi_{i,n} E_0 \left(\frac{LAI_{i,n}}{LAI_{max,i,n}}\right) A_{i,n}$$

$$I = \begin{cases} -k_S \Delta_{LAI} \Delta_I (\theta - 1)^{k_I} A_U & \text{if } I < P_U A_U \\ P_U A_U & \text{if } I \geq P_U A_U \\ U_c & \text{if } I > U_c \end{cases}$$

$$P_n = (P_t - I_{max} (LAI_n / LAI_{Lmax})) A_n$$

$$Q_{c2} = c P \text{ Area } Q_{c2}$$

$$Q_{out} = CL(H - HO)^{3/2}$$

$$\Psi_{i,n} = c_{i,n} \beta_{i,n} \alpha_{i,n} \Gamma_{i,n}$$

$$Q_{out} = Q_{out}$$

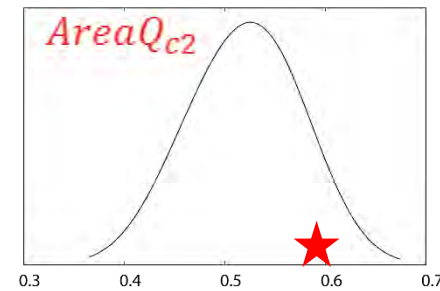
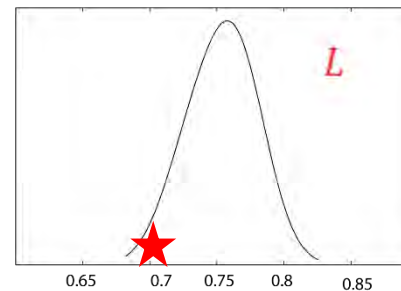
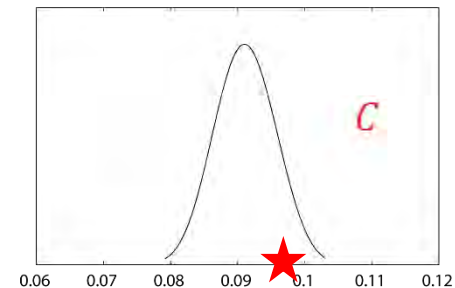
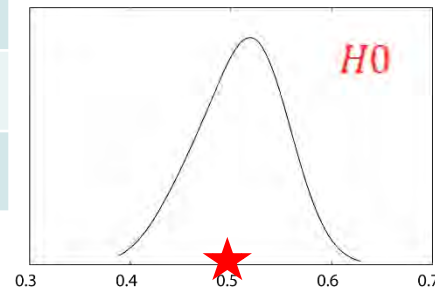
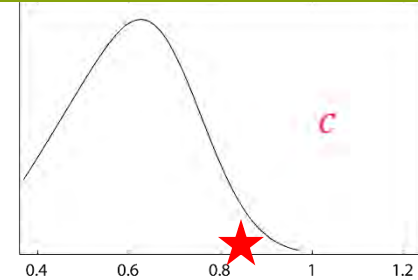
✓ Many ways to get it =



2a. Using WET0D with MCMC

Parameter	Initial Value	Minimum	Maximum
<i>Runoff Coeff.</i>	0.88	0.44	0.99
<i>Weir Coeff.</i>	0.1 (1.84)	0.05	0.15
<i>Area Mars St.</i>	0.6 km ²	0.3 km ²	1.2 km ²
<i>Width Weir</i>	0.7 m	0.35 m	1.4 m
<i>H0</i>	0.5 m	0.25 m	0.75 m

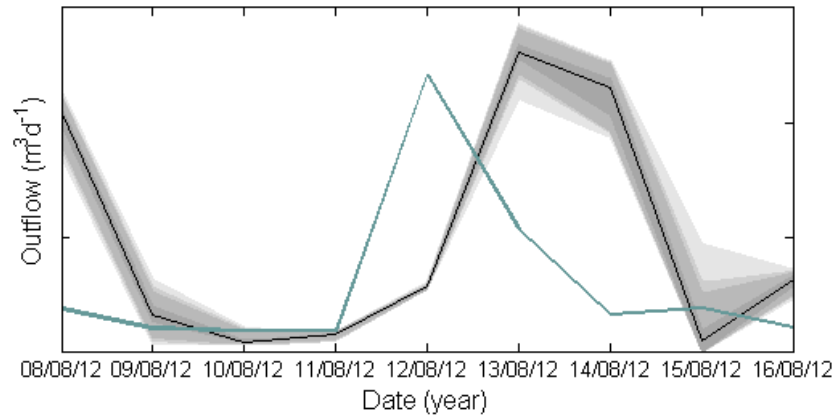
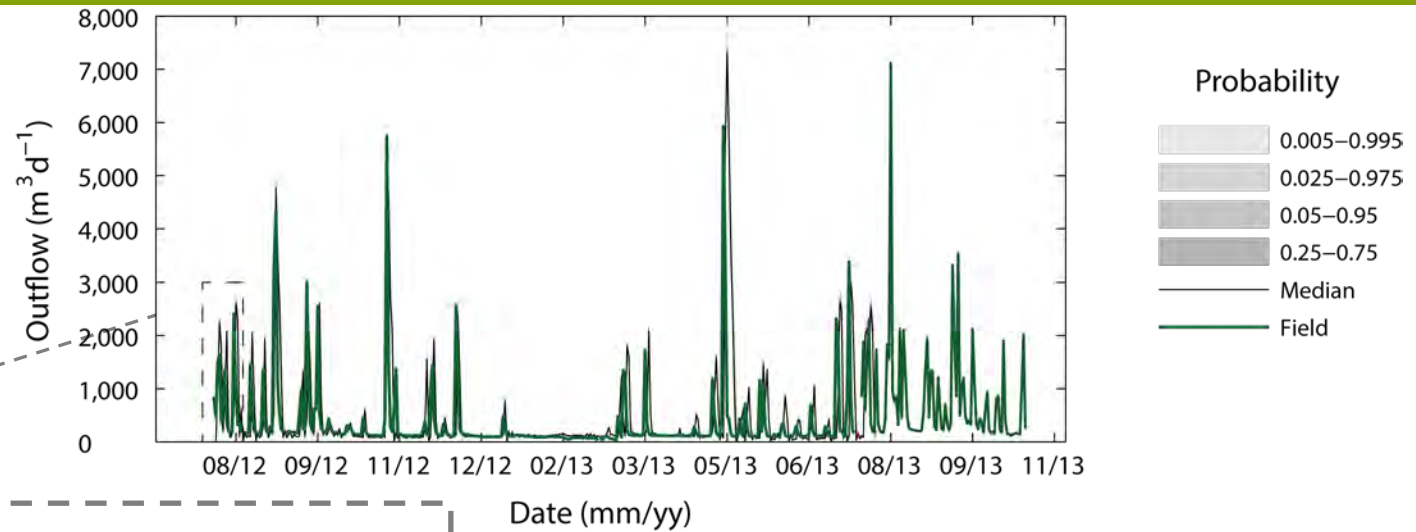
Probability
Distribution
Function of the
Parameters
Tested



$$RMSE (Q_{out}, Q_{out}) \gg 0$$



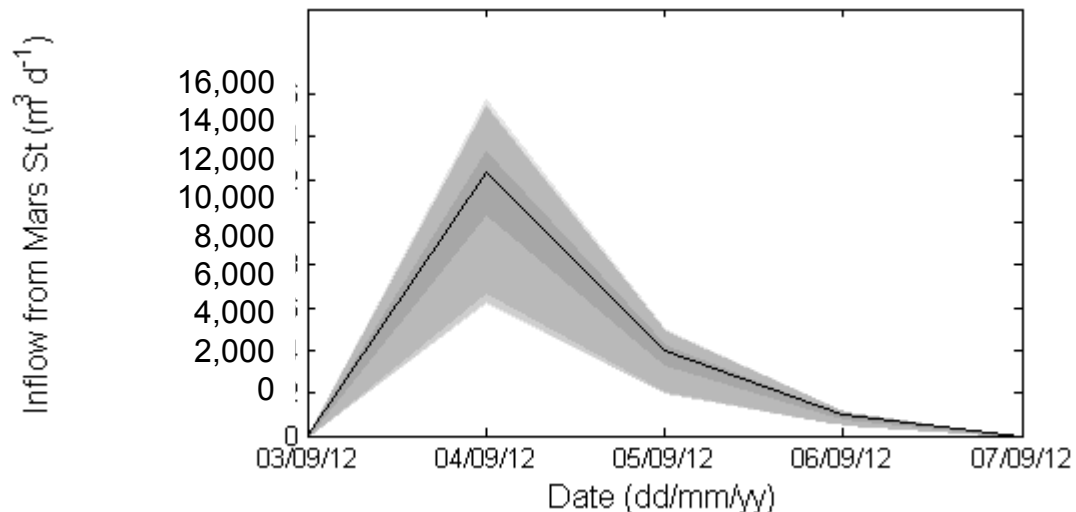
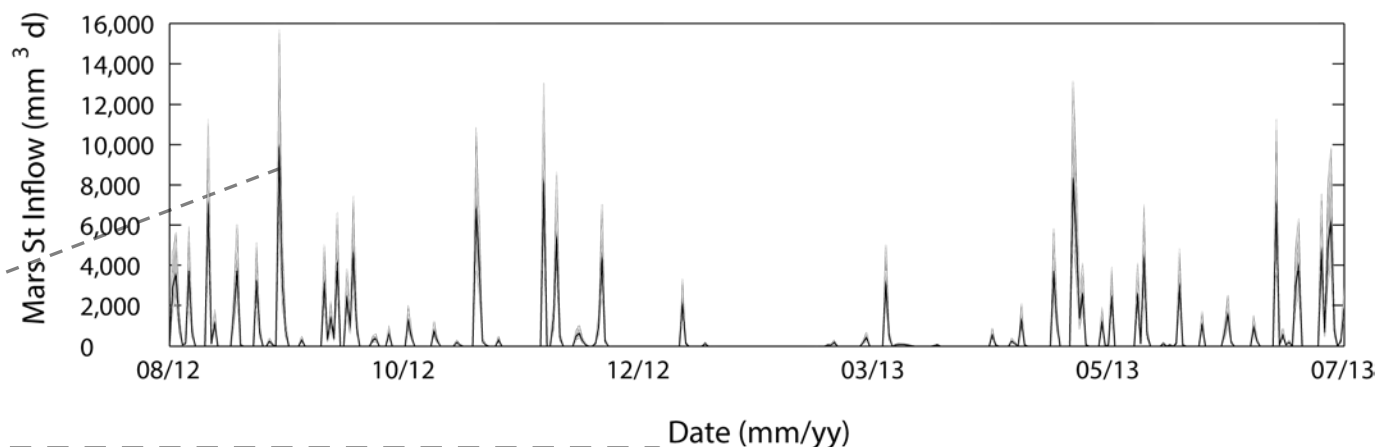
3. Preliminary Results



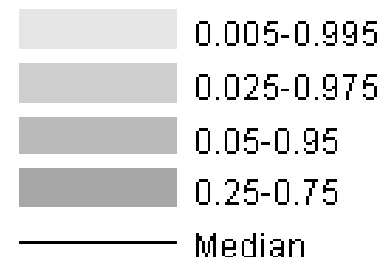
$$\text{RMSE} (Q_{out}, Q_{out}) \gg 0$$



3. Preliminary Results

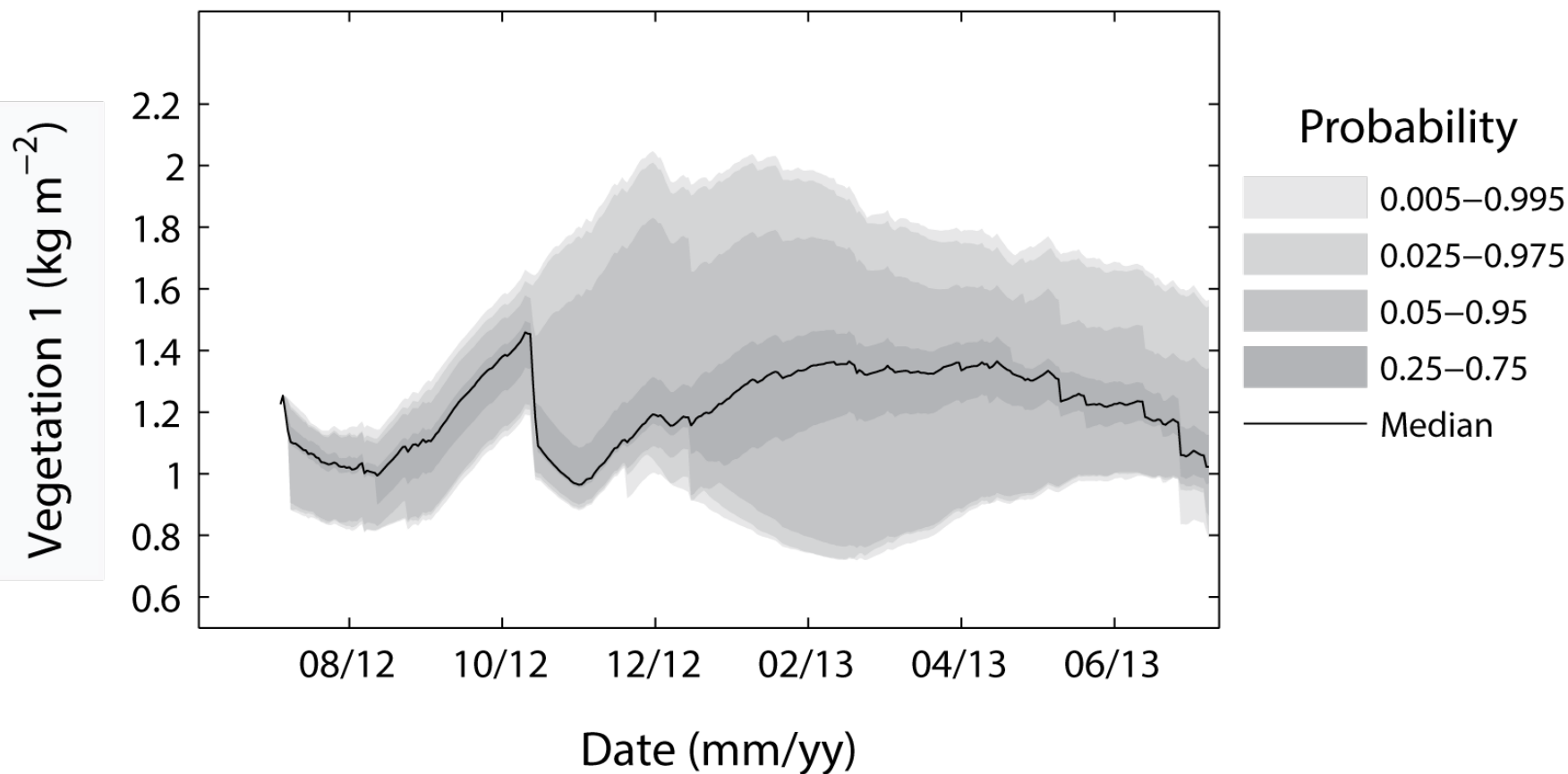


Probability





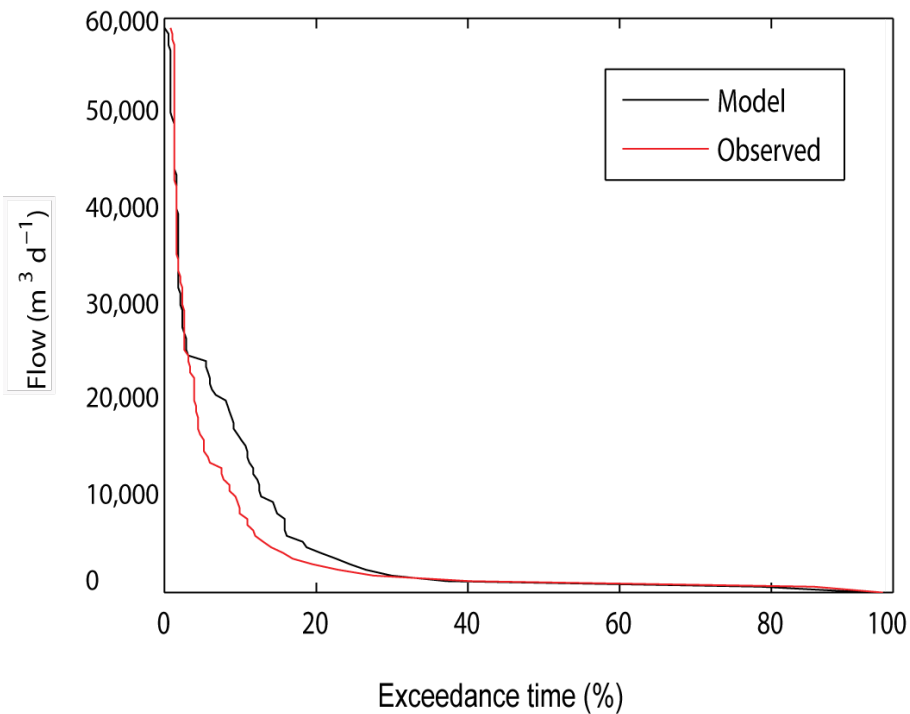
3. Preliminary Results



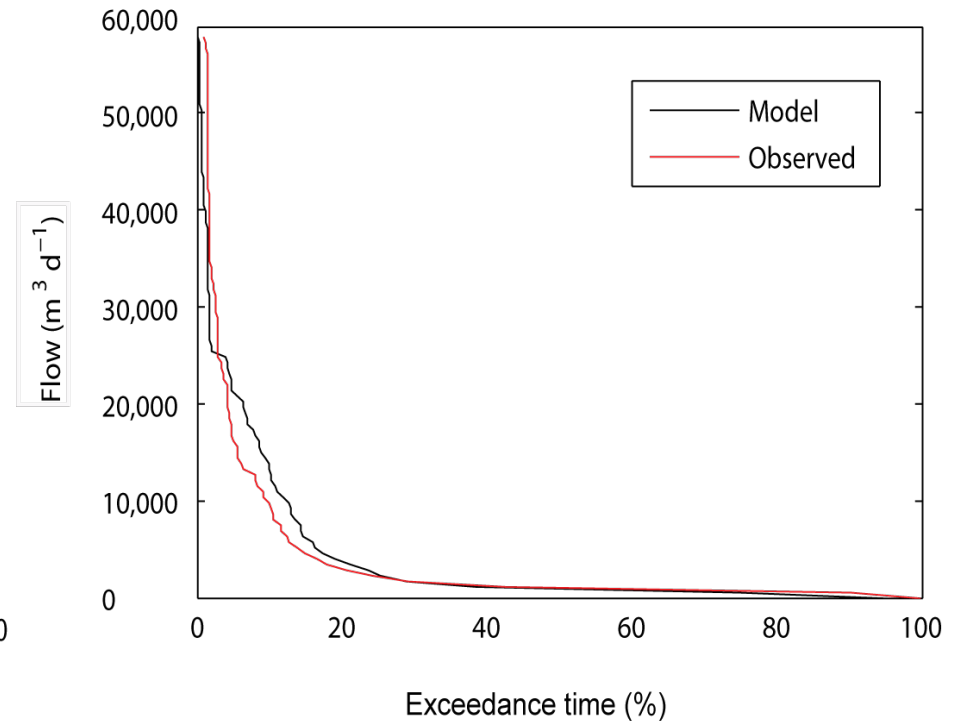


3. Preliminary Results

Before MCMC



After MCMC



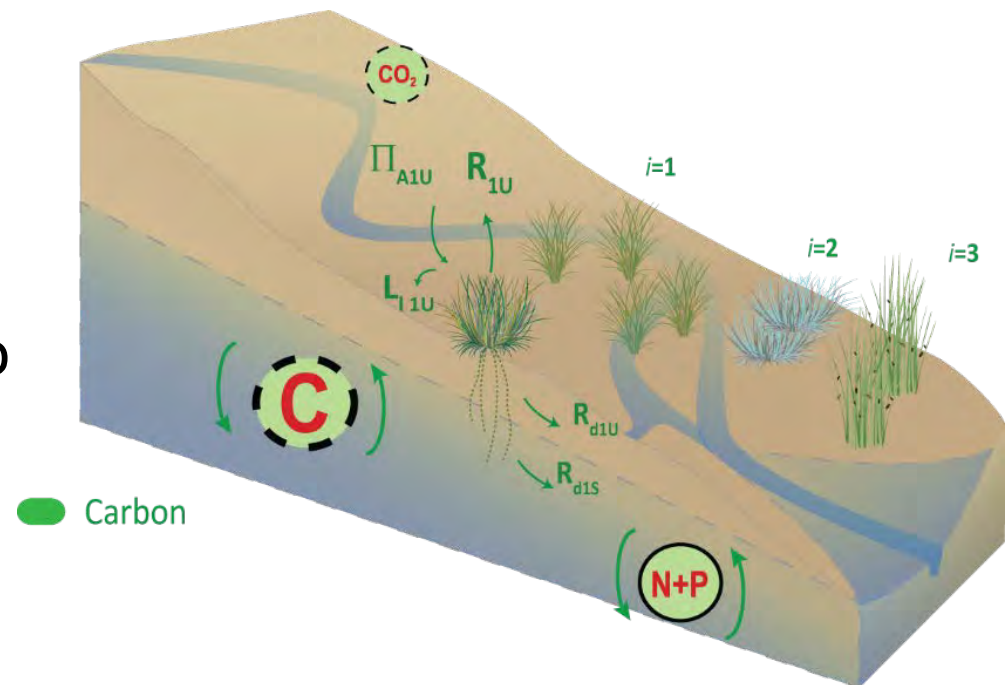


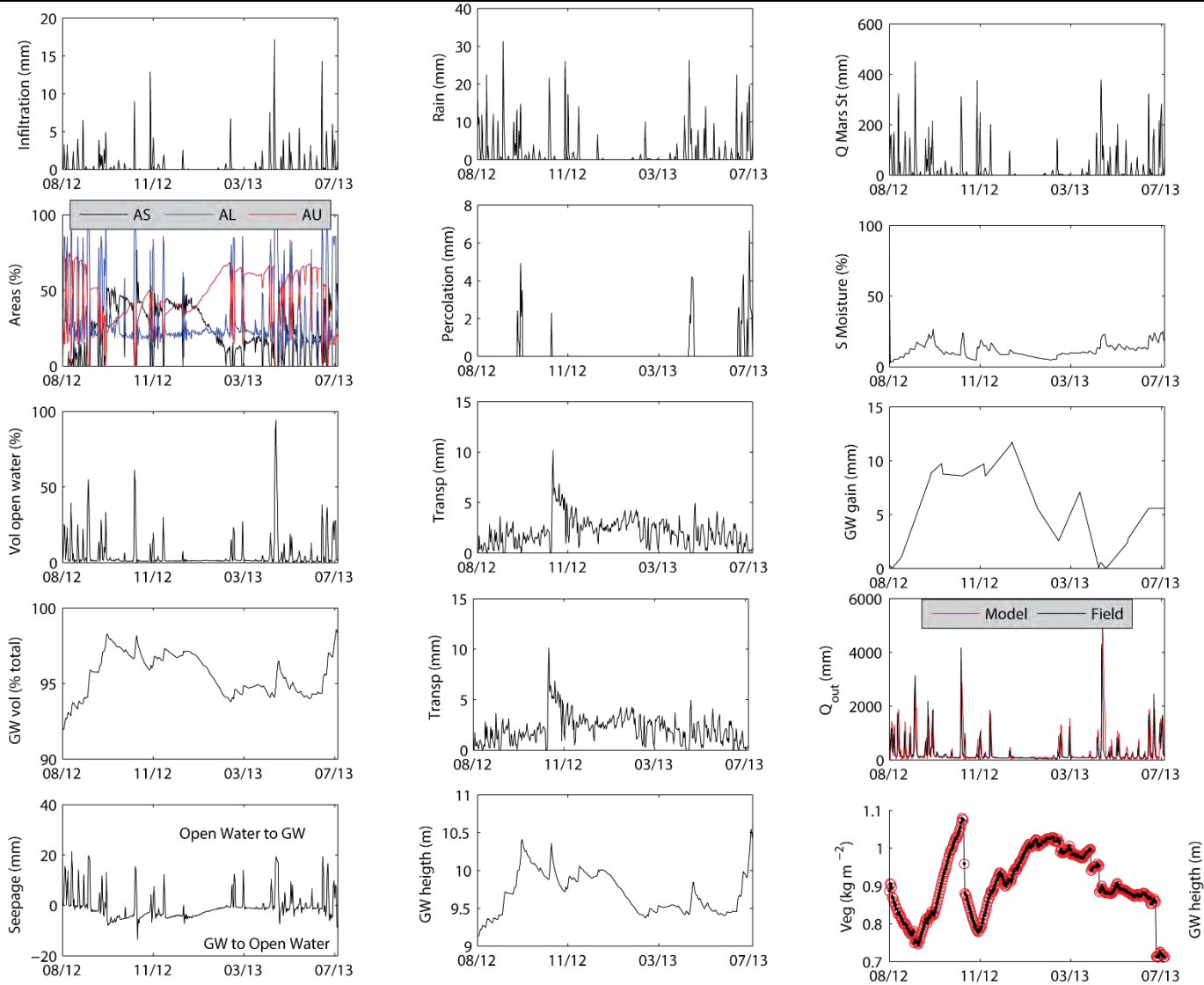
4. Next Steps

- ✓ Include biogeochemistry
- ✓ Validating vegetation biomass
- ✓ Hourly time-step
- ✓ Use within MCMC optimization framework to identify management effort to meet targets

Integrate with the General Lake Model (GLM)

Capture water, soil & sediment: C, N & P processing







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ARC Linkage Project LP110200975

From Where to Where?

UNRAVELLING PATHWAYS OF NUTRIENT FROM SOURCE TO SINK
IN URBANISING CATCHMENT

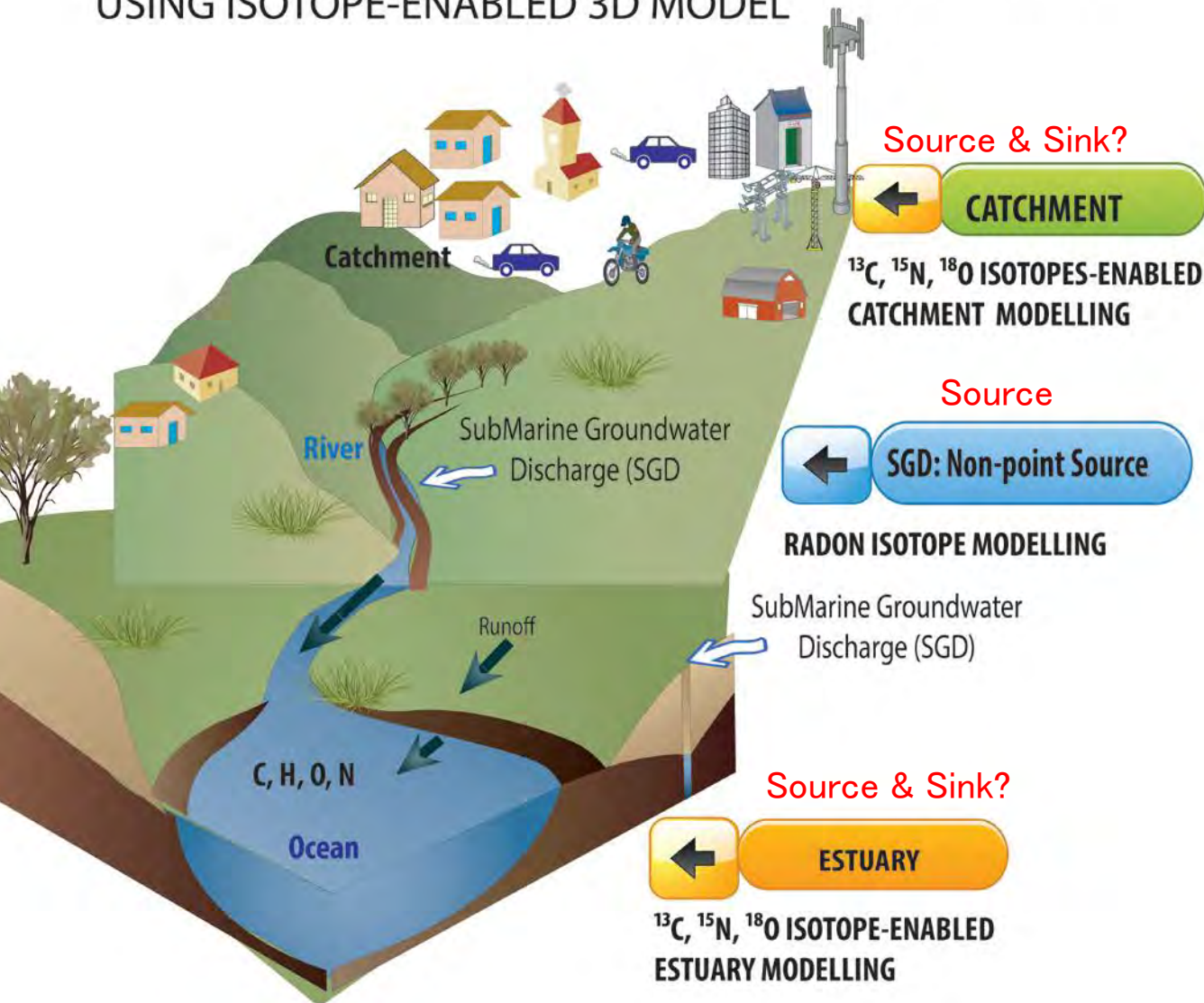


Sri Adiyanti^{*}, Bradley D. Eyre[#], Damien T. Maher[#], Isaac Santos[#],
Perrine Mangion[#], Meti Yulianti^{*}, Matthew R. Hipsey^{*}

^{*} Aquatic Ecodynamics, School of Earth & Environment, UWA, Crawley WA 6009, Australia.

[#] Centre for Coastal Biogeochemistry, Southern Cross University, Lismore, NSW 2480, Australia.

UNRAVELLING SOURCES OF NUTRIENT TO AN ESTUARY USING ISOTOPE-ENABLED 3D MODEL



Caboolture River Catchment



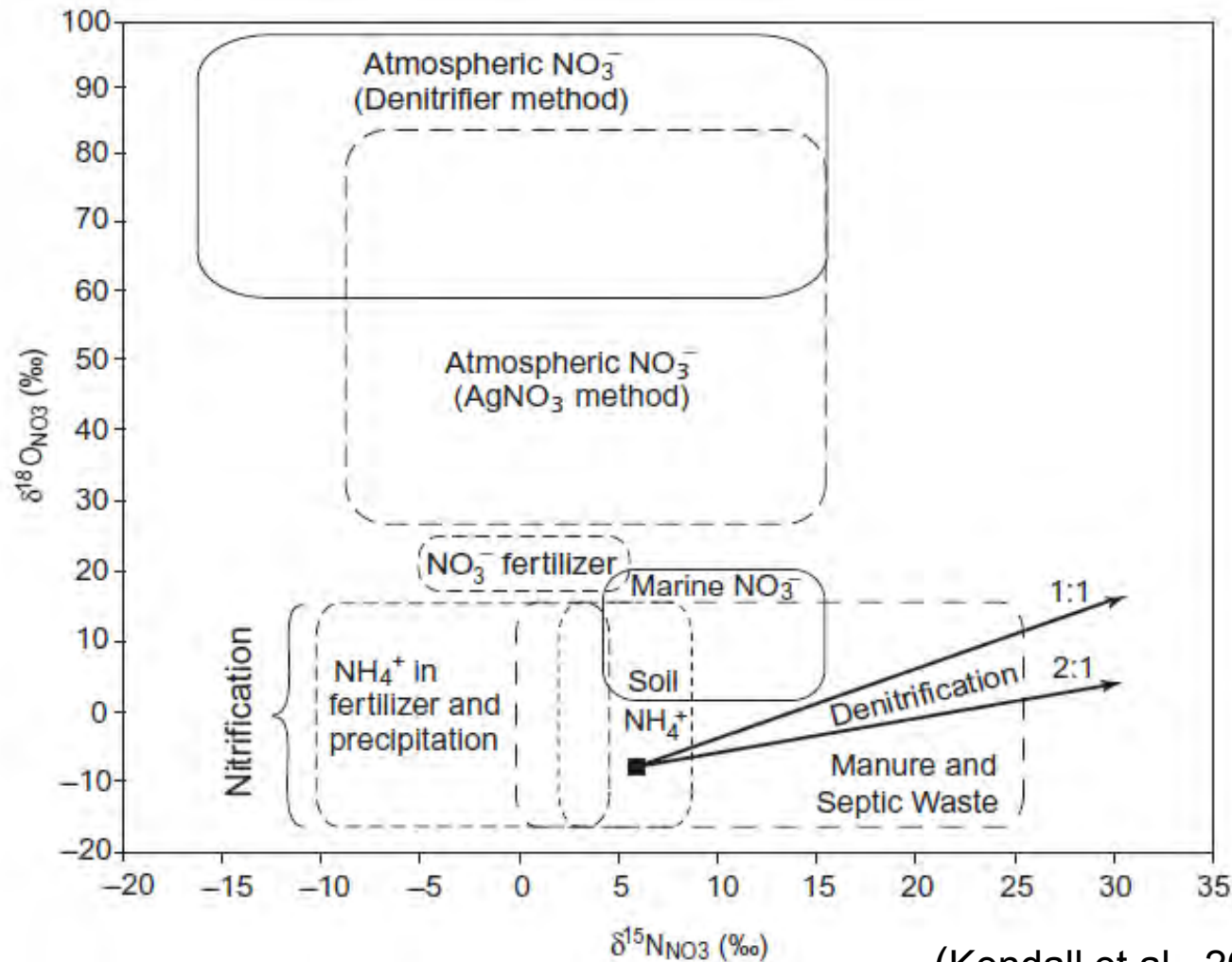


MOTIVATION

- ❑ Caboolture River Estuary WQ: steady decline due to:
 - Agricultural (?)
 - Industrial activities (?)
 - Urbanization (?)
- ❑ “Nutrient Accounting”: trace and identify nutrient pathways
- ❑ Acknowledge:
 - Large spatiotemporal variability in water quality of contributing environments and biogeochemical processes along freshwater-marine continuum, and this variability are not captured with routine monitoring programs. [Need to use 3-D Hydrodynamic Model]
 - Uncertainty in model results. [Need Bayesian Hierarchy Model]
- ❑ USING ISOTOPE-ENABLED 3-D HYDRODYNAMIC MODEL & BAYESIAN HIERARCHY MODEL

USING STABLE & RADIOACTIVE ISOTOPES SIGNALS as TRACERS of SOURCES and PATHWAYS

Typical Values of $\delta^{15}\text{N-NO}_x$ and $\delta^{18}\text{O-NO}_x$ (at source):



(Kendall et al., 2007)

Typical Values of $\delta^{222}\text{Rn}$:

GW: $10^2 - 10^3 \text{ Bq/m}^3$

SW: 10^1 Bq/m^3

Estuary: $10^{-2} - 10^2 \text{ Bq/m}^3$

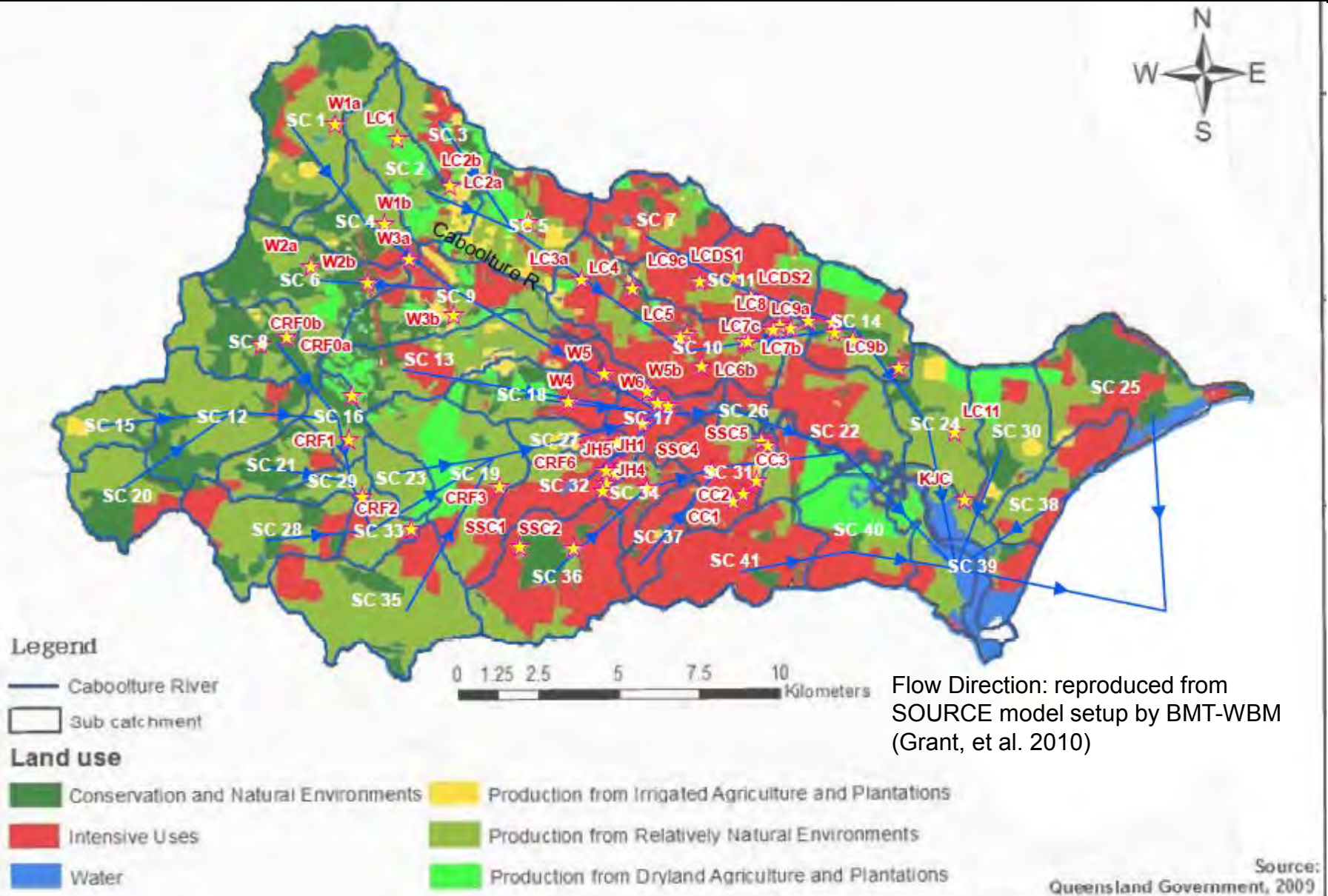
Data: Caboolture (2011-2013)



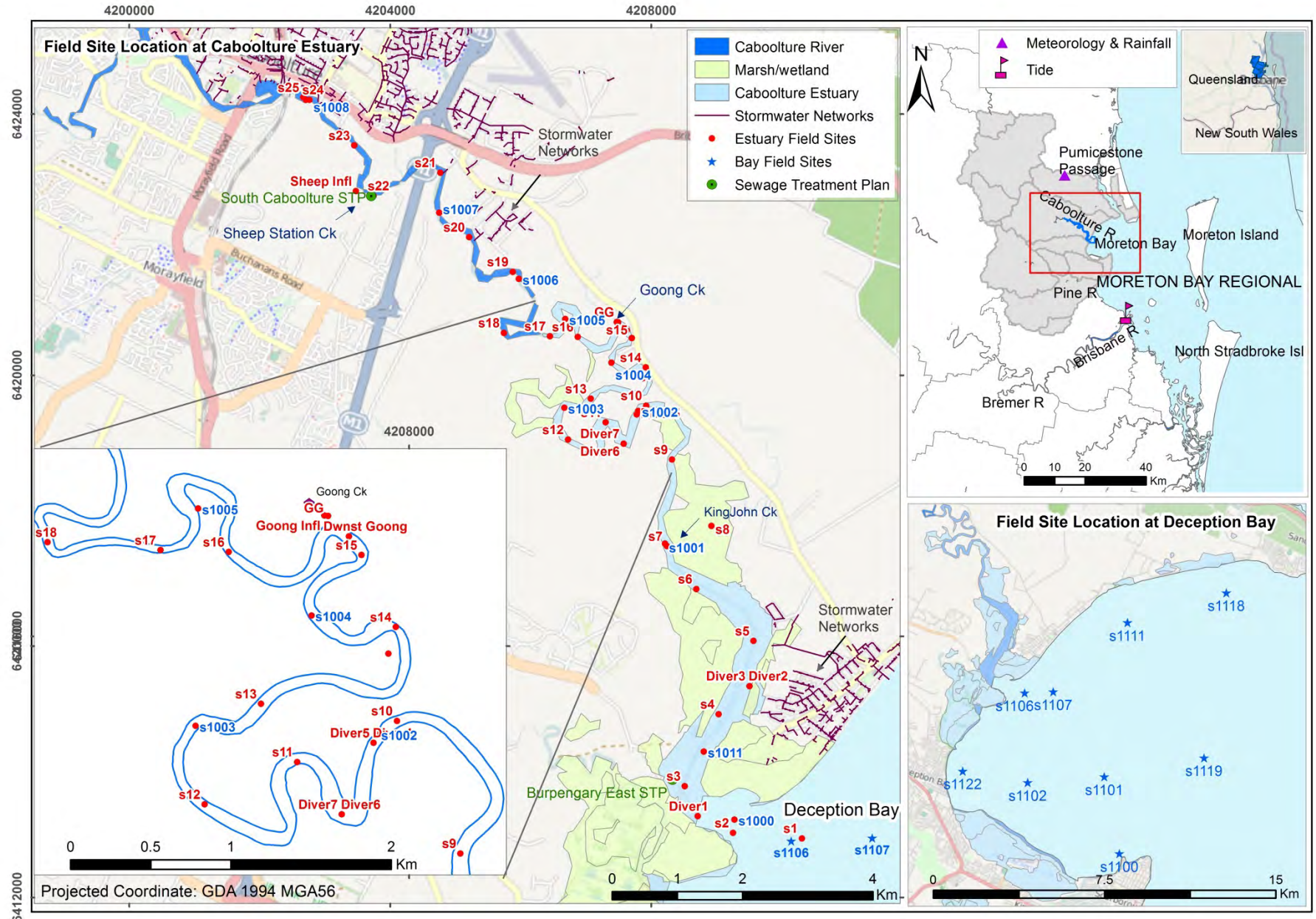
COMPREHENSIVE DATASETS: e.g.

- Southeast Queensland Ecosystem Health Monitoring Program (SEQ-EHMP) since 2000: physico-chemical, nutrient (Healthy Waterways, 2014).
- Centre for Coastal Biogeochemistry, Southern Cross University: physico-chemical, nutrient, chl-*a*, isotopes (2011-2013).
- South Caboolture & Burpengary WWTP Effluent Flow & Nutrient (2006-2014).
- Caboolture Shire Council: physico-chemical, nutrient, chl-*a*, metal (2001-2010).

CABOOLTURE RIVER CATCHMENT: LANDUSE & FLOW DIRECTION

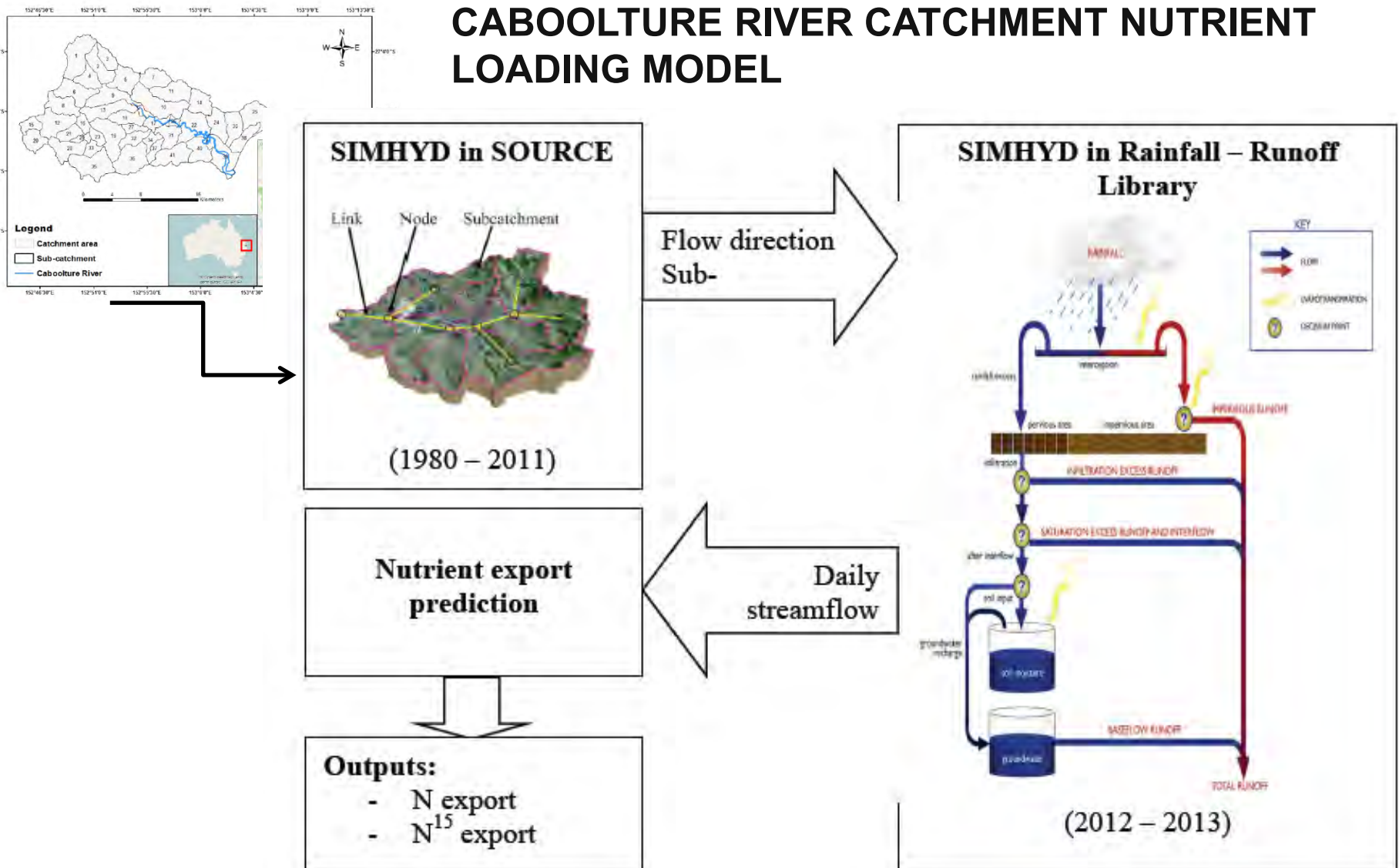


ESTUARY WATER SAMPLING LOCATION





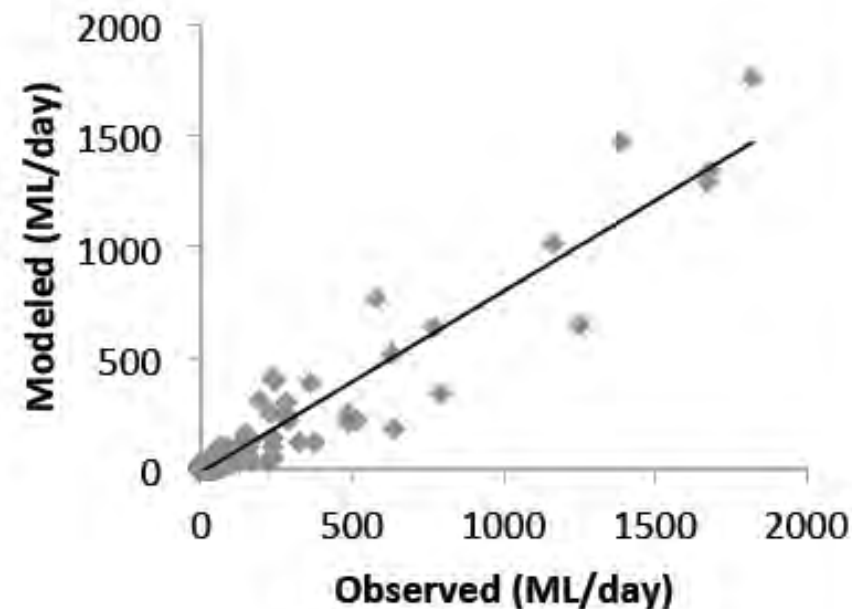
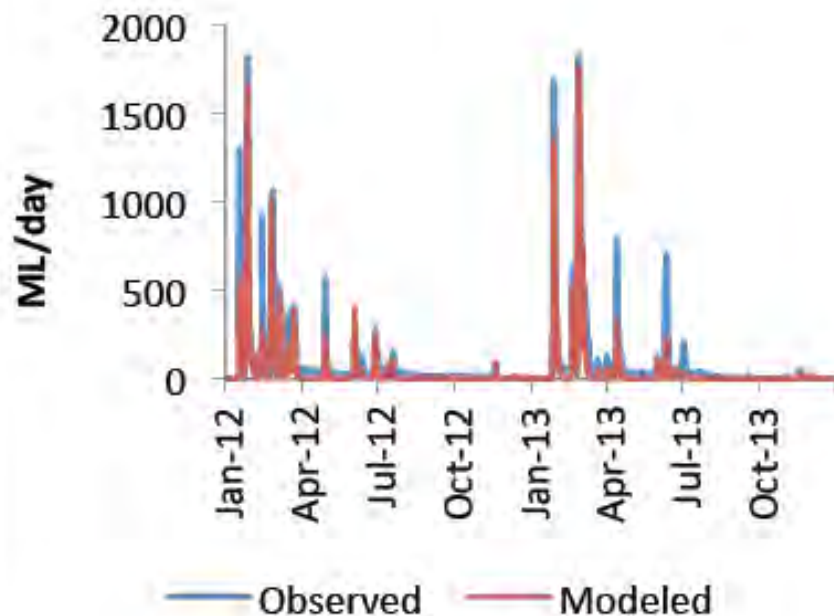
CABOOLTURE RIVER CATCHMENT NUTRIENT LOADING MODEL





Discharge at UpperCaboolture Gauging St:

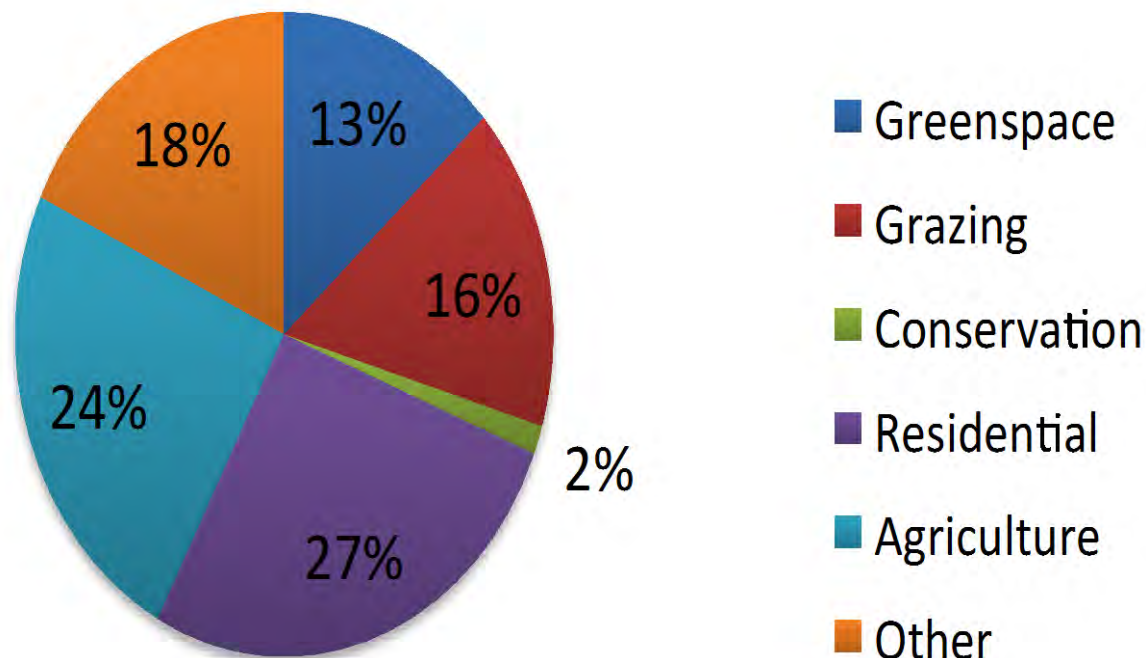
R^2 0.8705 and Nash-Sutcliffe coefficient of efficiency (NSF) of 0.89



(Yulianti, M. 2014)

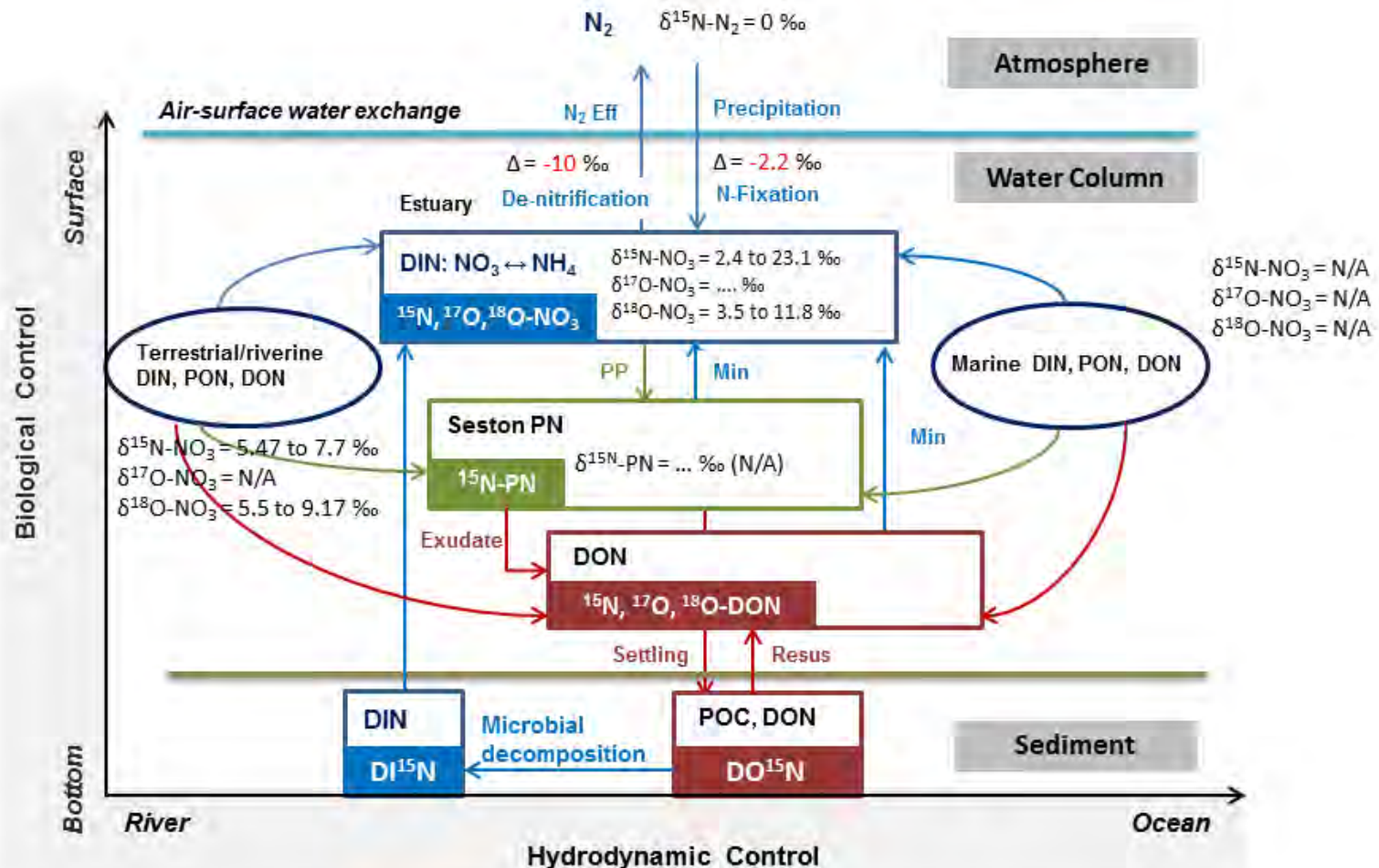
IF (ONLY) USING CATCHMENT NUTRIENT LOADING MODEL:

CABOOLTURE: SOURCE OF NUTRIENT (2012-2013) BASED ON LANDUSE:

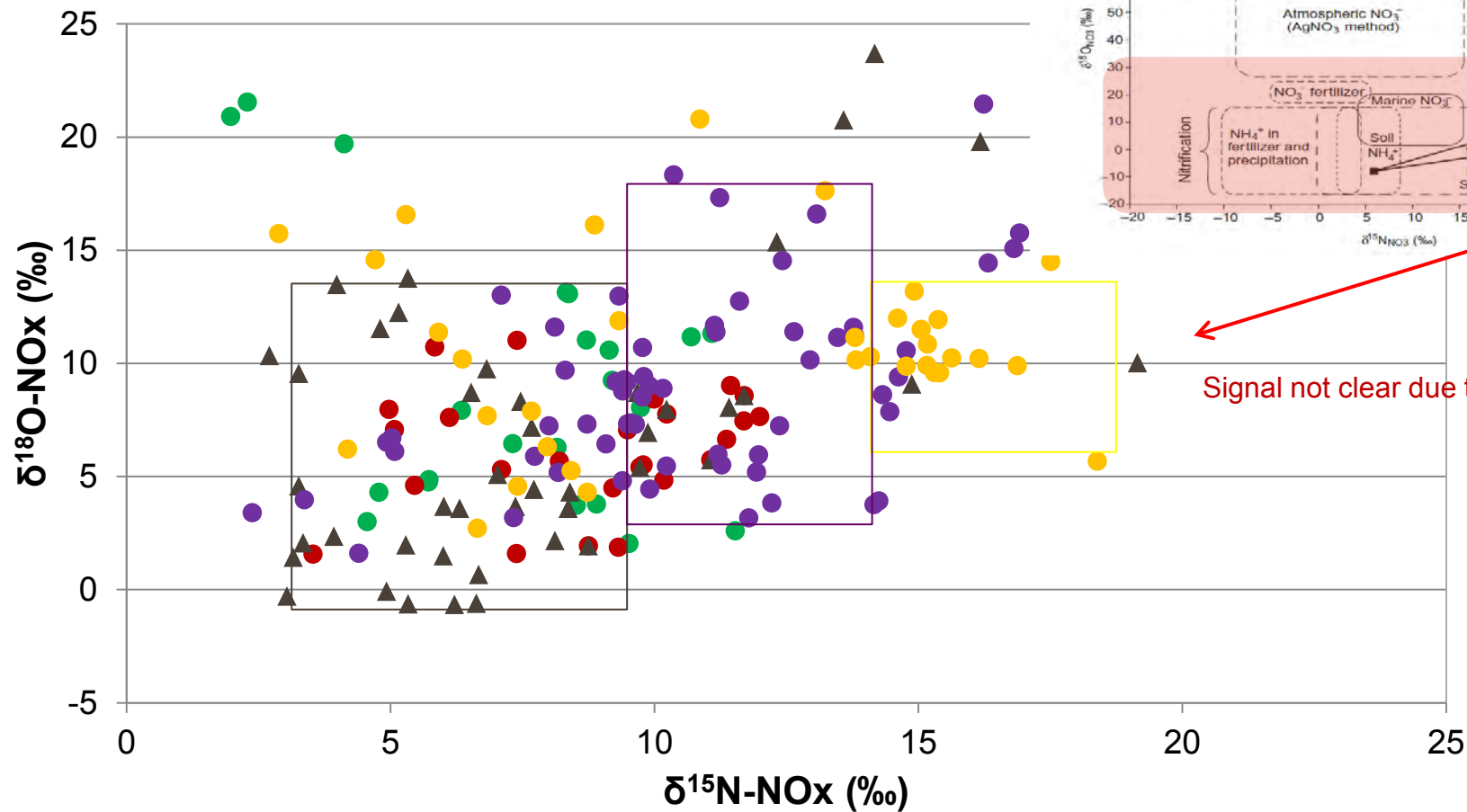


Modelled using SOURCE MODEL and NUTRIENT data

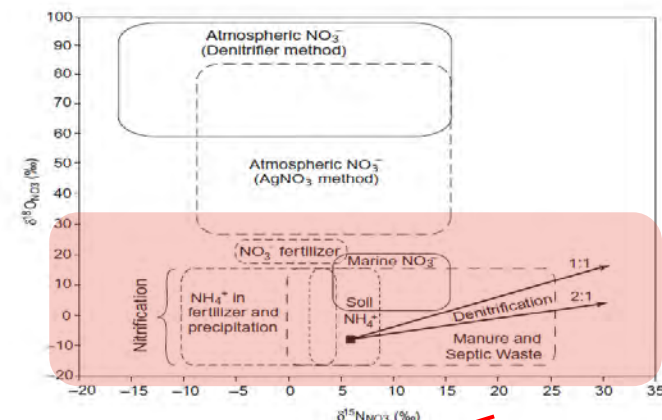
IF USING ISOTOPE-ENABLED 3-D HYDRODYNAMIC MODEL: We can trace nutrient pathways



Caboolture: Biplot Isotope Signature



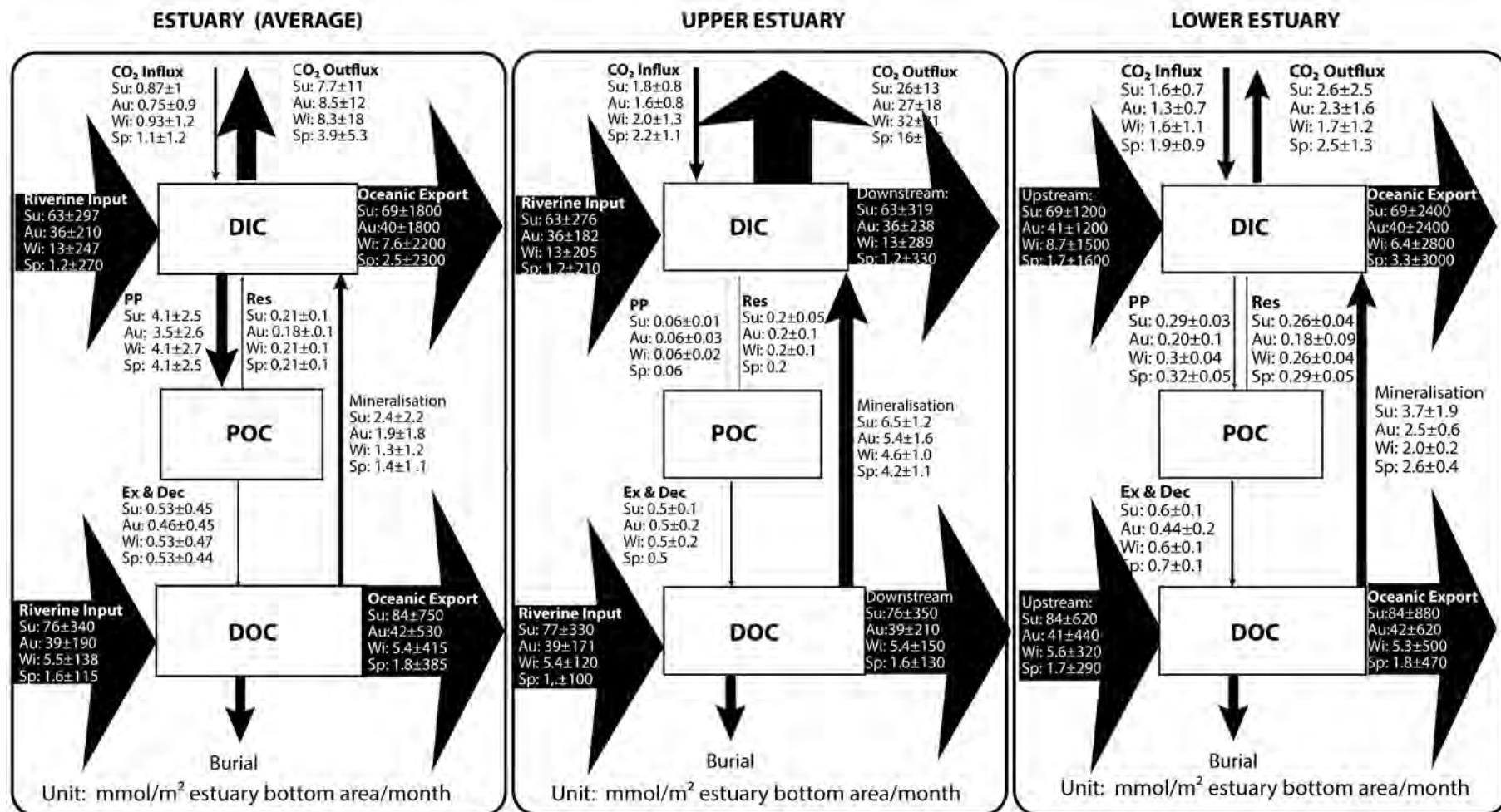
● Greenspace ● Grazing ▲ Conservation ● Residential ● Agriculture



Signal not clear due to isotope mixing

Example of Large Spatiotemporal Variability: Carbon Budget

based on $\delta^{13}\text{C}$ -DIC & $\delta^{13}\text{C}$ -DOC 3-D model result



[Adiyanti et al. (submitted) An isotope-enabled biogeochemical model combined with uncertainty assessment for quantifying carbon flux pathways in a salt-wedge estuary. A manuscript submitted to *Environ. Model. Softw.*, Dec 2014]



CONCLUSIONS:

ISOTOPE-ENABLED 3-D HYDRODYNAMIC MODEL & BAYESIAN HIERARCHY MODEL is a powerful tool to:

- ☐ trace and identify nutrient pathways;
- ☐ show spatiotemporal variability in WQ of contributing environments and biogeochemical processes;
- ☐ take into account uncertainty introduced in the model due to boundary condition, parameters, model description.



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THANK YOU...

